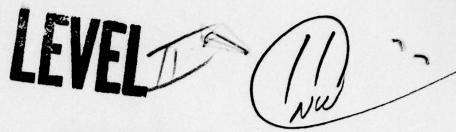
ARMY MISSILE RESEARCH AND DEVELOPMENT COMMAND REDSTO--ETC F/G 20/4 USER'S MANUAL FOR THE MARTIN-MARIETTA HIGH ANGLE OF ATTACK AERO--ETC(U) AD-A057 138 JUN 78 G C WINN DRDMI-T-78-63 UNCLASSIFIED NL 1 of 1 AD57 138 END DATE FILMED 9 = 78 DDC



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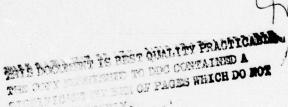
USER'S MANUAL FOR THE MARTIN-MARIETTA HIGH ANGLE OF ATTACK AERODYNAMIC METHODOLOGY FOR BODY-TAIL MISSILES

Gary C. Winn Aeroballistics Directorate Technology Laboratory

U.S. ARMY
MISSILE
RESEARCH
AND
DEVELOPMENT
COMMAND

**JUNE 1978** 

WELLER WAY



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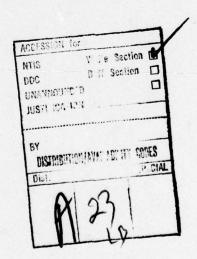
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US Army Missile Research & Development Command
Attn: DRDMI-TI June 1978 NUMBER OF PAGES Redstone Arsenal, Alabama 35809

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### I. INTRODUCTION

The Martin Marietta Corporation, Orlando Division, has developed an aerodynamic methodology and published a report (Ref. 1) under Contract No. DAAHOl-74-C-0621 with the US Army. The report describes the development and application of semiempirical methods for predicting aerodynamic characteristics of slender body and body-tail configurations.

In an effort to evaluate the Martin Methodology, a computer program was developed to incorporate the various theoretical and empirical procedures called for in the Martin report. The results of this evaluation are covered in detail in Ref. 2. As a follow-up to the Martin Methodology analysis, a few modifications of the methodology were accomplished in an attempt to correct certain disagreements found between measured experimental data and associated predictions derived from the methodology.

This report is intended to be a user's guide for the use of the methodology program. The methods and procedures used in developing the aerodynamic methodology are covered extensively in Ref. 1 and only those modifications to the methodology implemented by the Army will be discussed in this report.

### II. PROGRAM CAPABILITIES

sweep angle

The Aerodynamic Methodology Program can predict aerodynamic characteristics of slender body and body-tail missile configurations, to include the following predictions:

- 1) Body alone normal force, center of pressure, and axial force.
- 2) Isolated tail panel normal force and center of pressure.
- 3) Mutual interference effects that enable the prediction of normal force and center of pressure of body-tail combinations.

The program in its present form was developed to predict these characteristics for missiles with four fins in cruciform configuration, with the fin trailing edges flush with the missile body base. The fin numbering convention, as well as the conventions for angle of attack  $(\alpha)$  and roll angle  $(\phi)$ , are shown in Figure 1.

The range of input parameters for the program are:

1) Mach number 0.8 to 3.0

2) Angle of attack 0 to 180 for isolated components (roll angle = 0). 0 to 45 for body-tail combinations at arbitrary roll angles from 0 to 180.

3) Tail leading edge 0 to 70 degrees

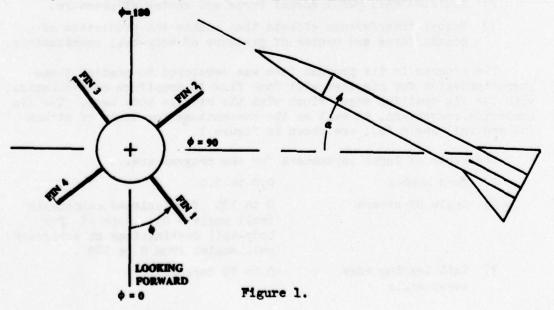
4)	After-body length (calibers)	6 to 18
5)	Nose length (calibers)	1.5 to 3.5
6)	Tail taper ratio	0 to 1
7)	Tail aspect ratio	.5 to 2.0 (aspect ratio of two tail panels joined at root chord)

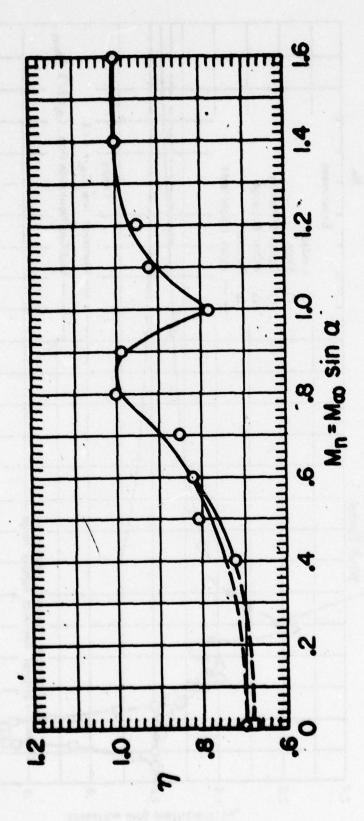
### III. DISCUSSION

Certain modifications of the original methodology were incorporated into the methodology computer program. These modifications were an attempt to correct certain disagreements between experimentally obtained data and associated predictions from the methodology which became apparent during an evaluation of the original methodology (Ref. 2).

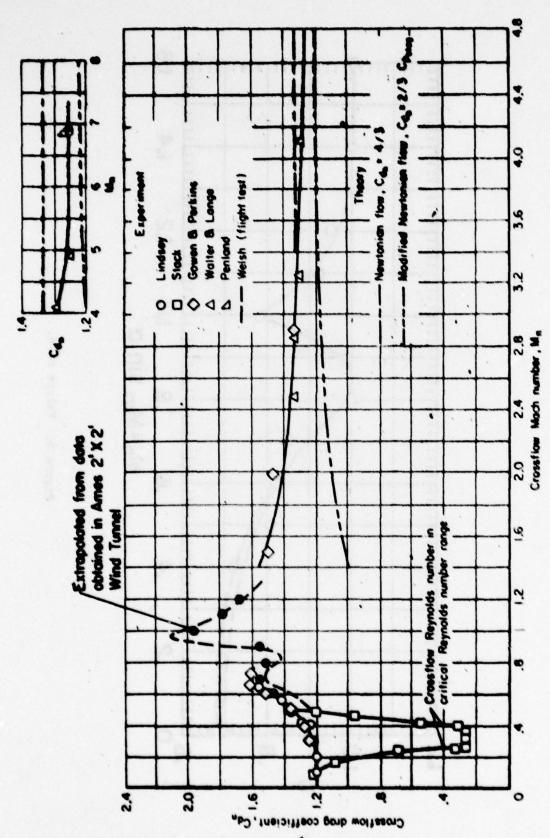
The modifications are limited to the body alone normal force prediction methods and involve the addition of newly obtained unpublished data. Specifically, equation 16, page 36 as depicted in Figure 20 of Ref. 1, has been eliminated and replaced by values of  $\eta$  (correlation factor for end effects) as shown in Figure 2 of this report. In addition, the crossflow drag coefficient versus crossflow Mach number curve shown in Figure 22a of Ref. 1, has been replaced by Figure 3 of this report.

Comparisons of predictions generated from the original methodology and those with the above modifications, compared with the experimental data, are shown in Figures 4 through 10 of this report.





Pigure 2. Values of n.



Pigure 3. Unpublished data.

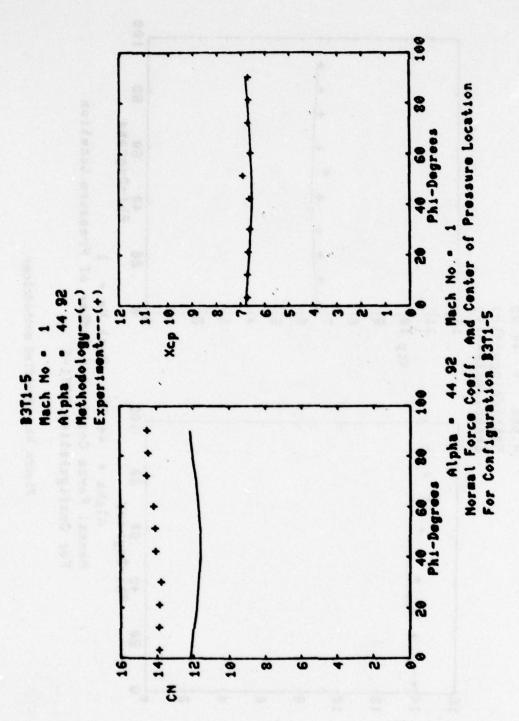


Figure 4a. Original methodology.

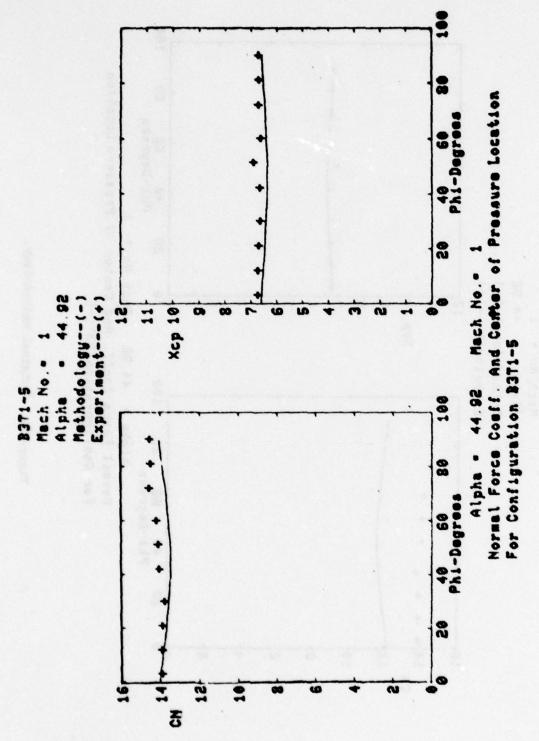


Figure 4b. Modified methodology.

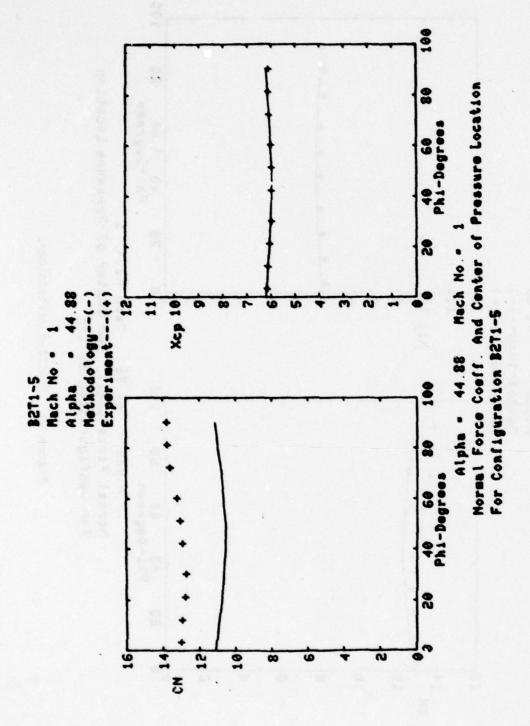


Figure 5a. Original methodology.

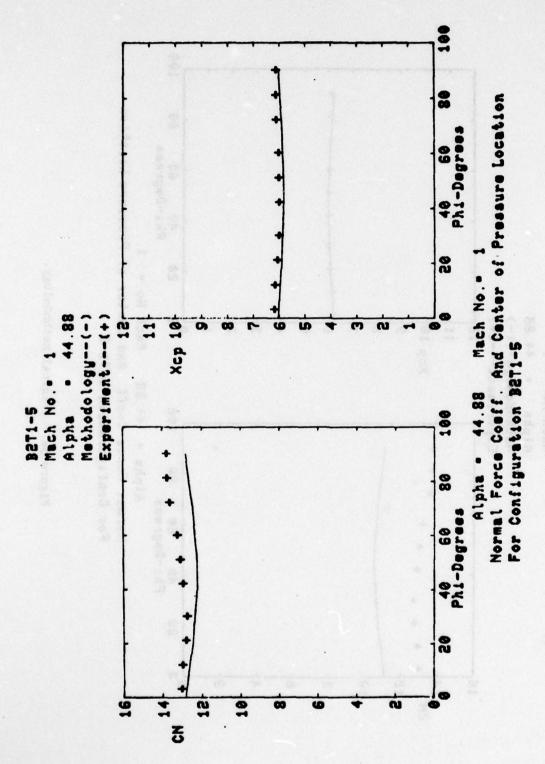


Figure 5b. Modified methodology.

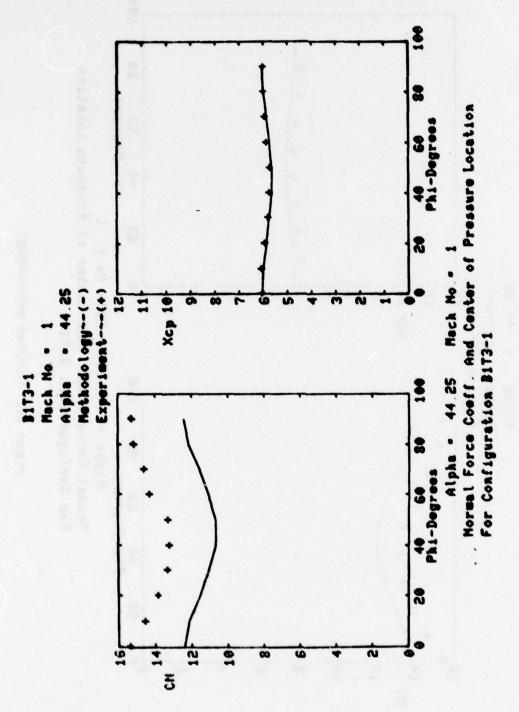


Figure 6a. Original methodology.

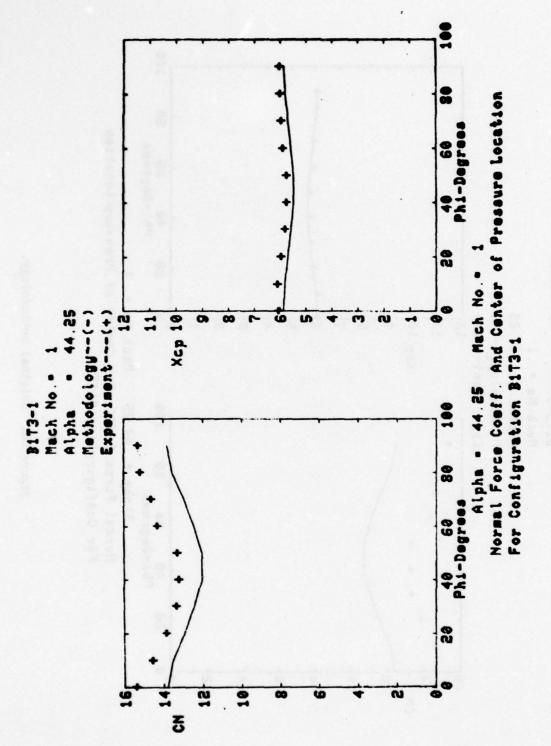


Figure 6b. Modified methodology.

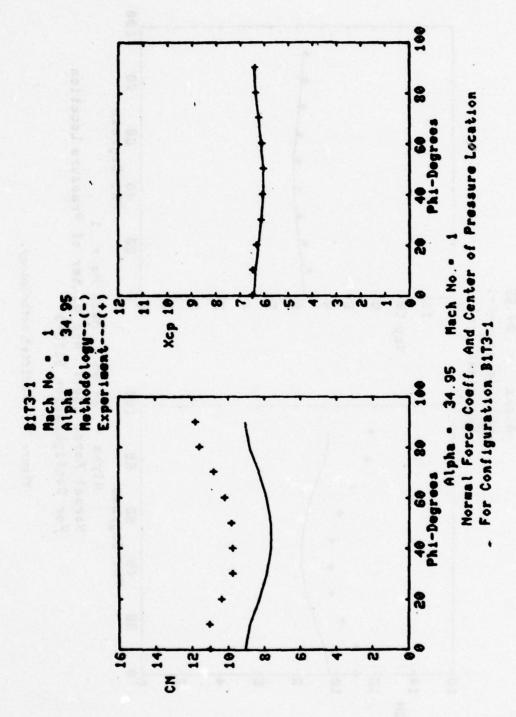


Figure 7a. Original methodology.

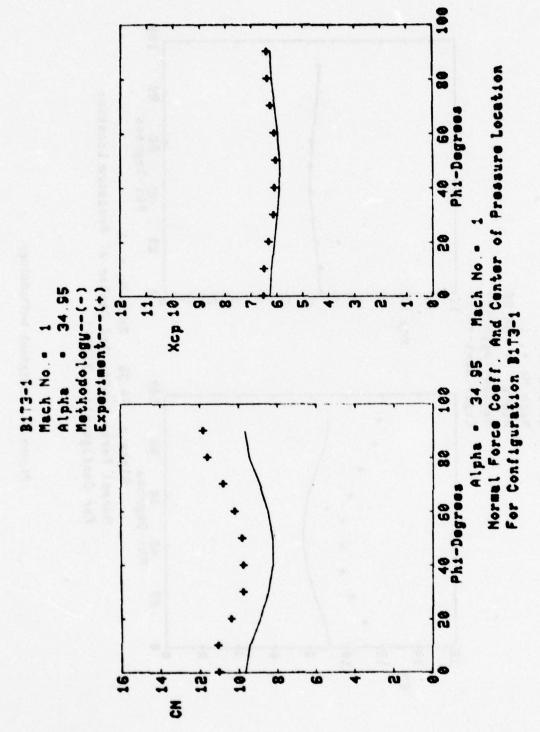


Figure 7b. Modified methodology.

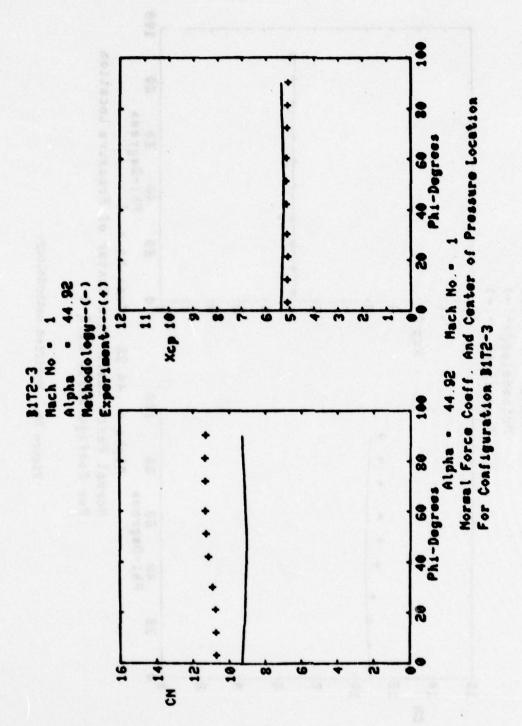


Figure 8s. Original methodology.

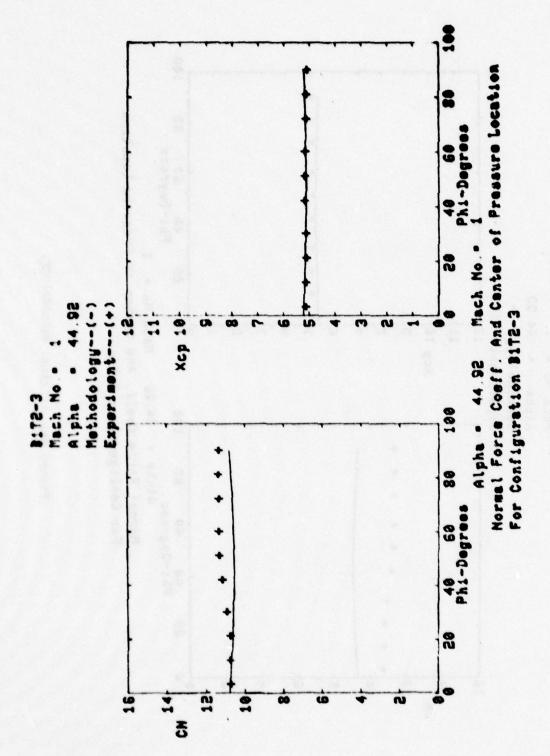


Figure 8b. Modified methodology.

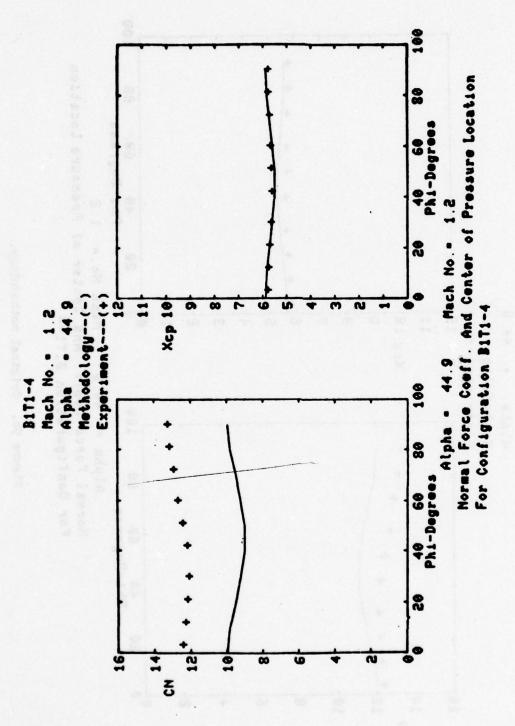


Figure 9a. Original methodology.

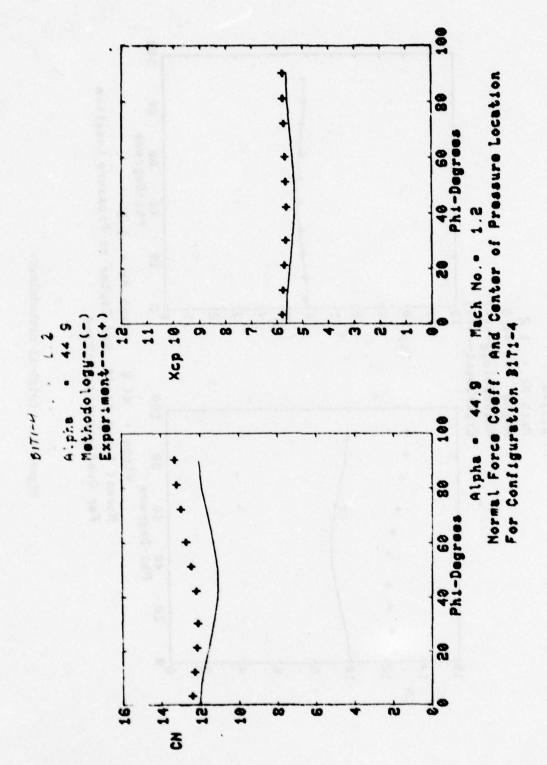
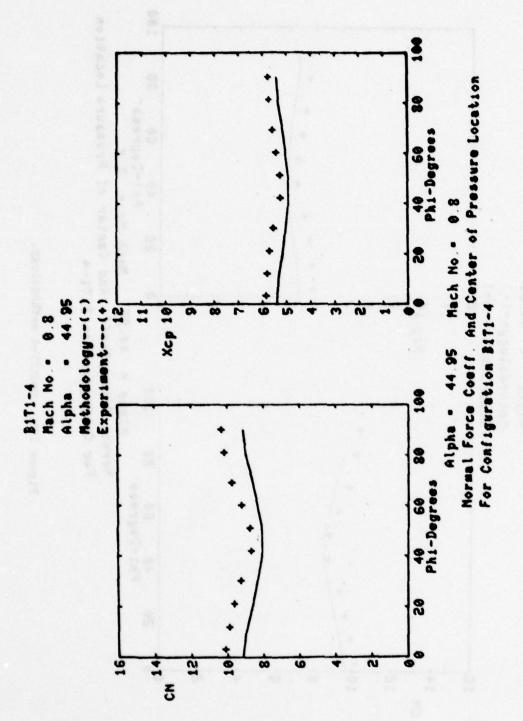


Figure 95. Original methodology.



Pigure 10a. Original methodology.

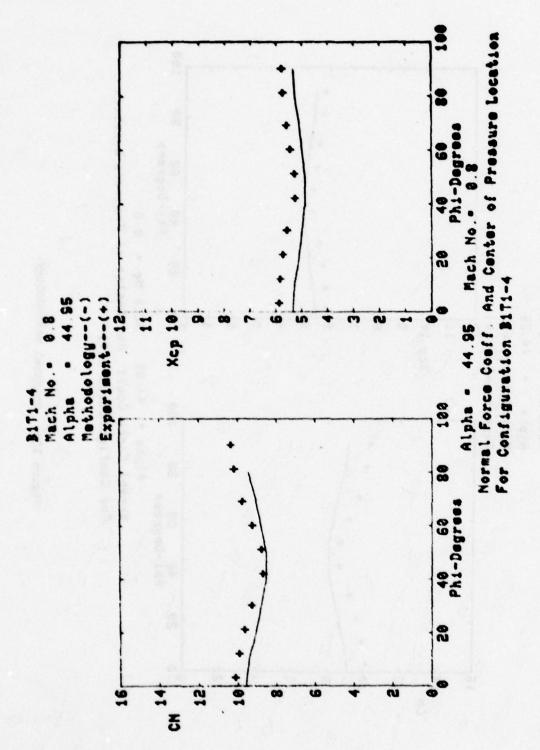


Figure 10b. Modified methodology.

## Appendix A. PROGRAM UTILIZATION

The proper format and sequence for the input cards are shown in Table A-1.

TABLE A-1.

CARD	SYMBOL REFERENCE	FORMAT (FORTRAN)
1	Title card for each configuration	12A6
2	AR,S,CR,LAMDA,ALE	5F10.3
3	LND, LAD, D	3F10.3
4	ALF1, ALF2, DELAF, MACH, RN, OPTPHI, OPTMAC	4F10.3,F13.2,212

AR = Tail aspect ratio (two tail panels joined at root chord)

S = Tail Semispan including body, (b + D)/2, inches

CR = Tail root chord - Inches

LAMDA = Tail taper ratio

ALE = Tail leading edge sweep angle - Degrees

LND = Nose length - Calibers

LAD = After-body length - Calibers

D = Body diameter - Inches

ALF1 = Beginning angle of attack for angle of attack sweep - Deg.

ALF2 = Ending angle of attack for angle of attack sweep - Deg.

DELAF = Angle of attack increment for alpha sweep - Degrees

MACH = Free stream Mach number

RN = Reynolds number - /Ft.

OPTPHI = 1 to calculate aerodynamic coefficients as a function of roll angle. Roll angle is automatically varied between 0° and 90° in increments of 10°. No additional data cards are required. See Sample Configuration 2 Input Data.

 0 to delete calculation of aerodynamic coefficients as a function of roll angle

OPTMAC = 1 allows for multiple Mach numbers for the configuration and angle of attack range determined by the four cards Table A-1. Additional Mach numbers are added after the four cards of Table A-1, one Mach number per card using F10.3 Format

- 0 for single Mach number only

### MULTIPLE CASE CAPABILITY:

Additional configurations can be input simply by repeating the card sequence of Table A-1.

If OPTMAC = 1, however, a blank card must follow the last Mach number card before the program will accept additional configurations.

Table A-2 shows a sample input card arrangement. Using this input card arrangement the program will predict aerodynamic coefficients for sample configuration No. 1 for Mach No. equal .8 and for angles of attack from 0.0 to 45. degrees in 5 degree increments. Since OPTPHI is 0 for sample configuration No. 1, the coefficients will be given versus angle of attack only (roll angle equals 0 degrees). Now, OPTMAC equals 1, therefore additional predictions will be made for the same configuration and angle of attack range for Mach numbers: .9, 1.0, 1.1, 1.2, and 1.3. A blank card follows the Mach number cards for sample configuration No. 1, which signals the program to read additional configurations.

The program then reads the cards for sample configuration No. 2, and computes the predictions of the aerodynamic coefficients and centers of pressure for this configuration. Now, since OPTPHI equals 1 in this case, these predictions will be given as a function of roll angle, for the angle of attack range 0 to 40 degrees. Also, since OPTMAC equals 0 for this case, the predictions will be made for Mach No. equal 2.0 only.

The resulting output for these sample input cards are found in Table A-3.

As a guide for time and storage requirements, the following figures for the CDC 6600 are provided:

Compile Time - 14 seconds

Execution Time - 2 seconds

Storage - Less than 100K.

# FORTRAN - 7090 CODING FORM

TIRE:	TABLE A-2.
CODER:	Identification DATE
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SAM	1. S.A.M.P. L.E. C.J.N.F.L.G. U.B.A.T.I.S. 1
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2.6.7	
1 1 1	
1 1	
1 1 1	
1 1 1	
	1 4 1 4 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1

-		
	INPUT	INPUT PARAMETERS
	MACH	
	TAIL	ASPECT RATIO = 1.00
	TAIL	TAPER RATIO = 0.00
	TAIL	L.E. SWEEP ANGLE = 75.96 DEGREES
	TAIL	-
	NOSE	NOSE LENGTH = 3.000 CAL.
	AFTE	AFTER BODY LENGTH = 7.000 CAL.
	BODY	BODY DIAMETER = 3.75
	TAIL	TAIL SEMI-SPAN(INCLUDING BODY) = 3.75
	REYNC	REYNOLDS NUMBER = 7000000.00

CNB = BODY ALONE NORMAL FORCE COEFFICIENT  XCPB= BODY ALONE CENTER OF PRESSURE  CNT = TAIL ALONE NORMAL FORCE COEFFICIENT  IXCPT= TAIL ALONE CENTER OF PRESSURE  CNT(B)= TAIL (IN PRESENCE OF BODY) NORMAL FORCE IN  COEFFICIENT  COMFIGURATION (IN PRESENCE OF BODY) CHORDWISE IN  CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED IN  AFT FROM ROOT CHORD LEADING EDGF)  YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE IN  CENTER OF PRESSURE/TAIL SEMICE OF BODY  CONFIGURATION (CAL. FROM BODY  CONFIGURATION (CAL. FROM NOSE)  CNT(BOT)= NORMAL FORCE COFFICIENT OF BODY  IN PRESSURE COMFICTENT OF BODY  CNT(BOT)= NORMAL FORCE COFFICIENT OF BODY  IN PASSURE COMFIGURATION  IN PASSURE		
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000	.888			6699	.620	.863	.613	.316	2.651		7.394		.169
000	1.151			906.	.616	1.020	.617	.301	3.219		7.281		141
.00	1.652			-234	.611	1.236	.623	.282	4.081		7.042		.093
00.	3.695	3.927		1.220	.617	1.219	.630	.282	6.168		6.026		.019
000	5.701			1961	.622	.975	.637	.282	7.908		5.386		081
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INPUT PARAMETERS  MACH = "90  TAIL ASPECT RATIO = 1.00  TAIL L.E. SWEEP ANGLE = 75.96 DEGREES  TAIL ROOT CHORD = 7.500  MOSE LENGTH = 3.000 CAL.  AFTER BODY LENGTH = 7.000 CAL.  BODY DIAMETER = 3.75
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XCPT=	TAIL	ALONE	CENTER		PRES	PRESSURE	,		
CNT(B)=	_	TATLEIN	PRESENCE OF	30 33		BODY ! NO	BRAL	NORMAL FORCE	111
COE	COEFFICIENT	ENT							5000
XCPT(B) =	1 = 1	AIL C	TAIL IIN PRESENCE OF	SENCE	10	BODY)		CHORDUISE	2000
CENT	ER OF	PRES	CENTER OF PRESSURE/TAIL ROOT	AIL R		CHORD		CPEASURED	200
AFT	AFT FROM	ROOT	CHORD LEADING	LEADI		£ 06£ )			70.00
TCPTEB	PT(8) = TAIL	A11.	(IN PRESENCE OF	SENCE		BOOT	_	SPANNISE	1
CENTER		PRES	OF PRESSURE/TAIL SENI-SPAN	AIL S	EHI-	SPAN	CEXC	CEXCLUDING	1963
XCP (8+1)=		CENTER OF	OF PR	PRESSURE OF	10 3	BODY	FLUS	IS TAIL	
60		EASUR	MEASURED OUTBARD		FROM				
CONF	CONF I GURA	ATION	וניור.	FROM	NOSE				
CRT(8+T)= NORMAL	T)= N	ORMAL	FORCE	COEFFICIENT	FICI	ENT	9 40	RODY	
PLUS	PLUS TAIL	CONF	CONFIGURATIO	NOI					110000
CA = A	AXIAL	FORCE	COFFFICIE	ICIEN					

AHAT	1	ISOLATEL	100 0	PONENT				800₹	OT TAIL CO	NF IGURATION				
	I CNB	I XCPB	-	CMT	_	KCPT	CNT(8)	I KCPT(8) I	-	I CN(8+1)	-	XCP(8+T)	_	3
00	0.000	"		0.000		.651	0.00	.651	.335	0.000		-		.305
00	.246			.143		.651	.207	849.	.335	.708		6.987		.298
00	+09.			.311		.644	.436	-633	.335	1.534		6.820		.275
00	. 894			164.		.632	.664	.619	.335	2.266		956-9		.238
00	.893		2	969.		.621	*98*	.613	.316	2.650		7.353		.168
55.66	1.195	3.635	2	.903		.616	1.017	-617	.301	3.254		7.197		.166
00	2.782			1,239		.612	1.241	•624	.282	5.213		6.319		.126
90	4.615			1.192		.618	1.192	.631	.282	7.050		5.675		-065
0.0	6.240		•	:66.		.623	1.004	.638	.282	8.482		5.242		018
00	8.114			1.218		.629	1.253	**9*	.282	10.701		5.126		-1120

IMPUT PARAMETERS MACH = 1 ASPECT RATIO = TAIL LEST SEEEP AN TAIL REGIS CHORTH = 3.00 AFTER BODY LENGTH FALL SPARKING REYNOLDS NOWERR = 7 REYNOLDS NOWERR = 7 REYNOLDS NOWERR = 7 REYNOLDS NOWERR = 10.00 M M M M M M M M M M M M M M M M M M		- 1			1		. :				1	:	;
1.00 ASPECT RATIO = 1.00 TAPER RATIO = 0.00 L.E. SWEEP ANGLE = 75.96 DF6 REOT CHORN = 7.500 LENGTH = 3.000 CAL. PRODY LENGTH = 7.000 CAL. OIMMETR = 7.000 CAL. OIMMETR = 7.000 CAL.		œ	503										
ASPECT RATIO = 1.00  TAPER RATIC = 0.00  R.C. C. SLEEP ANGLE = 75.06 OF 5.  R.COT C.	MACH												
TAPER PATIC = 0.00 L.E. SWEEP ANGLE = 75.96 DFG RCOT CHORTH = 7.000 CAL. 0 DAMFTER = 7.000 CAL. 0 STAFFER = 7.000 CAL. 0 CON LENGTH = 7.000 CAL.	TAIL		FAT	0		1.0	0						
L.E. SWEEP ANGLE = 75.96 OFS RGOT CORAT = 7.500 LENGTH = 7.000 CAL. 01AMETER = 7.000 CAL. 01AMETER = 7.000 CAL. SCRIT SAAKINCLUDING EODY) = SCRIT SAAKINCLUDING EOOY) =	TAIL	TAPER	ATI		0	.00							
RCOT CHORD= 7.500 LENGTH = 3.000 CAL. R BODY LENGTH = 7.000 CAL. 01AMETER = 1.75 01CS NUMBER = 700000.00	TAIL	1.6.	433		375	"	75	90.	õ	3	33		
LENGTH = 3.000 CAL.  R DODY LENGTH = 7.000 CAL.  OIMMETR = 7.75  SCHILSPAKCHACLUPING EDRY = 5000 NUTS NUTS = 700000.00	TAIL	PC01	-040		1.5	00							
BODY LENGTH = 7.000 CAL.  DIAMETER = 7.75  SFMI-SPACINGLORNS BODY) = LOS AUMEER = 7000000.00	NOSE		**	000		AL.							
DIAMETER = 1.75 SEMI-SPANCINGLUDING BODY) = DLDS NUMBER = 7000000.00	BETE	R SOOF	SW.	H	- 1	.00	0	CAL					
SEMI-SPAREINCLUDING BODY? =	¥008		11	-	.75								
REYNOLDS NUMBER = 7000000.00	TAIL	15-1435	3446	INC	COL	ING	4	100			. 7	4	
	REYN	OLDS NUM	839	"	1	000	00	0.0	0				

100	RODY	ALCN	w	NOR	PAAL		FOPCE		130	1 4	COEFFICIENT	N.T			
(0)	BODY	ALONE		CFNTFR	2		a	PRESSUR	SUF	-					-
CN1 =	TAIL	ALGNE		NORMAL	HAL	-	a	2	130	COFFFIC	CI	IENT			-
=140X	TAIL	ALON		CENTER	150	0	4	Las	SUF	1					-
CNTCEDE		TAILLIN	a	RESE	35	0 33	30	008	140	0.4	œ	HAL	0	FORCE	•
203	-	IENT													-
KCPTCE	CPT(6) = TAIL	TAIL	CIN	d	3 3 3	PRESENCE OF	4		90	REDRY		HOP	CHORDWISE	351	-
CENT	ENTER OF	44 4	PPESSURE/TAIL	JAE	114	11	ROOT	10	CHOR	CRC	-	73.	CMEASUR	038	-
147	AFT FROM	œ	GOT CHORD LEADING	108	1 0	143	NIC		13903	3					-
TCP TE		TAIL		a	530	IN PRESENCE OF	4	4	EO	EDUTI		N 7 d	SPANNISE	35	-
CENTER	FR O	OF PRESSURE/TEIL SEMI-SPAN	ESSI	JRE	111	11	35	-11	ds		fE	XCL	CO	EXCLUDING	-
XCP (E.		CENTER OF PRESSURE	43	40	9	155	18E	0.5	80	YOU		SITIO		TAIL	-
7		MEASURED	URE	0	UTL	AR	FR	.00	3	100					-
CONF	a	ATIO	N	-4		IL. FRO"		NOSE	-						-
CNT(8+1)=		MORMAL	AL F	FORCE	4	303	Issi		TENT	_	40	50	FOOY		-
PLUS	-	L CONF		ISURATIC	11	ON									-
1 = 43	FIIAL	FOR	33	COEFF	1 33	ICIE	THE								-

	SIN	STURBONEON	STREET COMPONENTS
PT I CATOR)	XCPT I	-	XCPT I
	652	652	0 659
	-652	-652	-149 -652
	.646	.646	110
	.635	.635	.505
	.624	.624	.703
-	. 620	. 620	.907 .620
	1 119.	1 119.	1.250 .616 1
-	.621	.621	1.147 .621
626 1.085	.626	-	.626
•	. 632	1 613	1 05.0

JAPLE C	AMPLE CONFIGURATION			TMACET					
	INPUT PARAMETER	AME TERS							
	141 ASP 141 ASP 141 LAP 141 LAP 161 LAP	MACH = 1.10 TAIL ASPECT PATTO = 1.00 TAIL TAPER FATTO = 0.00 TAIL L.C. SWEEP ANGLE = 1.10 MACH = 1.000 TAIL ROTH = 1.000	. :	36 01681					
	FTER 50 F0DY 011 TAIL SER REYNOLDS	AFTER BODY LENGTH = 7. FODY DIAMETER = 3.75 TAIL SEMI-SFAMINGLUD RETWOLDS BUNNERR = 7	ATTER EODY LENGTH = 7.000 CAL- EODY DIANETER = 3.75 TAL SEMI-SFAMINGLUDING FORY) REYNOLDS BUNNER = 7000000.00	H. 100 = 3.75					
	i i al i a	SNOT THE HITTONS	, s						
######################################	### ### ##############################	### ##################################	CAS = ECOY ALONE NORMAL FORCE COFFICIENT XCPS= 8007 ALONE CENTER OF PRESSURE XCPT = TAIL ALONE CENTER OF PRESSURE CAST = TAIL AND PRESSURE TAIL ROOT CHORD (MEASURE DE AFT FROY ROOT CHORD L'ASING FORD) ACTION OF TAIL SENSURE TAIL SENSOR SORDY CAST = TAIL AND MEASURE CONTROL FORD NOSE) CAST = ASING FORCE COFFICIENT OF POOY FLUX TAIL COMFIGURATION CAST = ASING FORCE COFFICIENT	FIGURENT FIGURENT NOWAL F NO CHESS OF PLUS OF PLUS OF PLUS	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				
ALP MA	owe con	ISOLATED I XOPB	COMPONENTS I CNT I	I 147%	CNT (B)	00a 1 (89193) 1	PODY TATE CONFISURATION I VCPT(8) I CN(8-T)	1 20	1 xCP(8+1
3.68	1 40	2.624	0.000	*53*	0.00.0	•654	335	0.000	
5.00	346.	2.788	.146	163.	113.		.335	1.517	6.9
3.0.0	5.63	3.555		629	993.	929.	5223	2.027	7.41
3.00	025	3.806		9696	. 653	. 623	515	2.399	6-37
3.98	3,746	3.520	12121	.621	1.188	.630	.242	6.121	6.04
20.00	5.437	4.162		.625	1.261	•636	.282	7.968	5.76
. 3.00	9.152	4.281	1.322	989.	1.397	244	.262	12.124	5.50

THE CONTINUE TOWN IN THE PROPERTY OF THE PARTY OF THE PAR																
	INPUT PARAMETERS	15	. a	1 4	AME	ETERS										
	-	3	**		MACH = 1.20	0										
	TA	TAIL	-	30	ECT	ASPECT RATIO =	E	0		1.00	0					
	1	=	-	4 P	Ex	TAIL TAPER RATIO =	10		0	00.0	-					
	TA	TAIL	-	4		L.E. SHEEP ANGLE = 75.96 DEGREES	4	ANG	37	**	7.	6.9	9	E	SPE	ES
	17	TAIL	œ	00	1 0	ROOT CHORD= 7.500	6		.5	00						
	ON	SE	-	2	GTH	NOSE LENGTH = 3.000 CAL.	*	000	U	1						
	AF	TE	œ	08	10	AFTER BODY LENGTH = 7.000 CAL.	19	I	1	.00	0	CA	:			
	80	40	0	1	HET.	BODY DIAMETER = 3.75	*	m	75							
	1	=	V.	H	1-5	TAIL SEMI-SPANCINCLUDING BODY) = 3.75	=	NCL	On.	INC	-	008	2	**		15
	RE	Y	10	OS	NC	RETNOLDS NUMBER =	•		1	300	300	7000000007	00			

		מסוגמו מבי	DEFINITIONS	2			
							_
CNB =	BODY	ALONE	NORMAL		FORCE COEFFICIENT	CIENT	_
XCP8=	BODA	ALONE	CENTER		OF PRESSURE .		_
CNT =	TAIL	ALONE	NORMAL		COEFFI	CIENT	-
XCP T=		ALONE	CENTER		PRESSURE		_
CNTE	CNT(B)= TAILCIN		PRESENCE	90	BODYS NORMAL	RMAL FORCE	_
00	COEFF 1CIEN	IENT					_
XCPT	8) =	TAIL (	IN PRES	KCPT(B) = TAIL (IN PRESENCE OF	6 00 Y	CHORDHISE	_
CEN	CENTER O	F PRES	SUREITA	OF PRESSURENTAIL ROOT	CHORD	CHEASURED	
AFT	AFT FROM	ROOT	ROOT CHORD LEADING		EDGE )		_
YCPT	TCPT(8) = TAIL		IN PRES	(IN PRESENCE OF	BODY	SPANNISE	_
CEN	CENTER O	F PRES	SUREZIA	OF PRESSURE/: AIL SEMI-SPAN	NEGS-	CEXCLUDING	
XCPCB	XCP(8+1)=	CENTER	SE PRE	CENTER OF PRESSURE OF	F BODY	PLUS TAIL	
an	6400	BODYS MEASURED	ED DUTUARD	ARD FROM	FOUT		
CON	FIGUR	ATION	CONFIGURATION CCAL. FROM	ROM MOSE	13		_
CNTE	*11:	CNT(8+T)= NORMAL FORCE	FORCE	COEFFICIEN	IENT	OF BODY	_
PLU	PLUS TAIL	L CONF	CONFIGURATION	NO			-
. 5	AXIAL	= AXIAL FORCE	COEFFICIEN	CIENT			_
							_

5	.526	.518	.495	.459			.387	.364	.332	-
XCP(8+T)	-	7.008	7.013	7.474	7.155	6.302	6.056	5.610	5.652	
-										
TGURATION CNCB+T3	0.000	.721	1.491	2.020	2.903	4.780	6.407	8.432	10.682	
TAIL CONF	.335	.335	.335	.335	.316	.301	.282	.282	.282	
100								,		
MCPT(6) I YCPT	.655	-652	.641	.630	•626	•629	.634	•639	**9*	
CNT (B) 1	0.000	-207	.431	6+9.	. 837	.978	1.147	1.252	1.345	
			-							
XCPT	.655	.655	.649	.640	.632	.628	.625	. 629	.633	-
13										
PONENT	0.000	.1.	.307	.486	.67	-869	1.145	1.255	1.340	
3-										
SOLATED	2.431	2.665	3.191	3.741	4.051	4.152	4.253	4.355	4.456	
15										
CNB	0.000	1 .245	.549	.645	1.159	2.751	4.082	5.911	8.002	
ALPHA	00	00	00	00	00	000	00	00.	00.0	

MPLE	CONFIG	AMPLE CONFIGURATION 1 OPTPHI=0. OPTMAC=1	-	OPTE	HI=0	. 00	MAC		
	INPUT	INPUT PARAMETERS	TERS		9				
	MACH	MACH = 1.30							
	TAIL	TAIL ASPECT RATIO = 1.00	RAT	= 01	1.0				
	TAIL	TAPER RATIO =	ATI		0.00				
	TAIL	L.E. SWEEP ANGLE = 75.96 DEGREES	433	ANGL		15.96	30 5	345	S
	TAIL		ORD	. 7.	500				
	NOSE			000	CAL.				
	AFTE	AFTER BODY LENGTH = 7.000 CAL.	ENG		7.00	D CAL	•		
	800 ¥	BOOT DIAMETER = 3.75	*	3.7	5				
	TAIL	TAIL SEMI-SPANCINCLUDING BODY) = 3.75	ANC	INCLL	DING	600			15
	REYM	RETNOLDS NUMBER = 7000000.00	838	"	7007	1.000	00		

|--|

-											
I THE		ISOLATED	COMPONENTS		1	4008	TAIL CONF	15			:
-	CNE	I ACPB		XCPI	CNT(E)	1 XCPT(B) 1	1 (8) 17	CNEST	I ACPUBATI	-	5
00	0.000			.656	0.000	959.	.328	0.000	-		.530
00	.245	"		.656	.200	.653	.328	.713	5.963		.522
00	.529			959.	.411	.642	.328	1.450	7.052		664.
00	1680	.,		.642	.619	.632	.328	1.989	7.503		.463
00	1.491	•		.633	. 805	.628	.315	3.199	6.913		.413
00	2.825	4.339	.865	.630	.954	.631	.302	4.828	6.369	-	604.
00	4.417	•		159.	1.116	•636	.287	6.707	6.06		.405
00	6.108	•		.631	1.237	1 +9*	.287	8.613	5.886		.395
00.01	7.536	•		6899	1.341	949.	.287	10.213	5.814		.379
00	10.281	•		.639	1.424	.650	.287	13.087	5.661		.356

INPUT PARMETERS

INPUT PARMETERS

MACH = 2.00

TAIL ASPECT RATIO = 1.00

TAIL LAPER RATIO = .50

TAIL LAPER RATIO = .50

TAIL ROOT CHORE = 5.00

NOSE LENGTH = 3.000 CAL.

GOOT DAMETER = 3.75

TAIL SEMI-SPANINCLUDING POOTY = 3.75

REYNOLDS NUMBER = 6.50000.00

CND = SOUT DEFINITIONS

KEPS= BODY ALONE CENTER OF PRESSURE

KEPS= BODY ALONE CENTER OF PRESSURE

KEPS= BODY ALONE CENTER OF PRESSURE

KEPS= TAIL ALONE CENTER OF PRESSURE

KEPS= TAIL (IN PRESENCE OF BODY) NORMAL FORCE

CENTER OF PRESSURE/TAIL WOOT CHORD LEADING

KEPS = TAIL (IN PRESENCE OF BODY) CHORDWISE

CENTER OF PRESSURE/TAIL WOOT CHORD LEADING

KENTER OF PRESSURE/TAIL SEN-SPAN (EXCLUDING

KENTER TAIL CONFIGURATION

PLUS TAIL CONFIGURATION

PHI I CNTGE I I FIN A I FIN 2 I FIN A I FORTED I KCPTR-TO I CNTGE I CN	* LPHA=	00.0													
FIN 2   FIN 4   UPPER   LOWER   LOWE	I bu I	-	CATCE	-		XC	_		1 YCP	1(8)	XCPCF	.13	-	CN(B+T)	1 CA
0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000		1 714	2 1 FIN		UPPER I	1000	I UPPER 1	4 -7	1 FIN 2	FIN 4	UPPER	1005			
00000000000000000000000000000000000000		0.00	0.000	-	.536	.536	.536	.536	104.	.407	-	1		000-0	.3
0.000 0.000 .536 .536 .536 .413 .407	10.	000-0	00000		.536	.536	.534	.536	.408	104.	-	-		00000	.3
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09		##17E(6.151)	D ve		06.4000	
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		WELTERG. 115)			000150	
		4917E(6.120)			000000	
		4817576-1213			000780	
10		49175 (6,122)			000000	
		LR1TF (6.123)			000000	
		481TE (6.124)			000000	
		.RITE (5.126)			00000	
15		WEITF (6, 127)			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
		1917F (6,161)			098000	
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		URITE (6,130)			000000	
90		WATTE (6,171)			2000	
		UP 1 TE (6.152)			00000	
		.9116 (6, 133)			000000	
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36		11 = .5.CP.	TT = .5.CP.(1 LAHDA).(5-0/2.)		066000	
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		SEATION STANDANCE	STASE		001010	
		44FTS = ((2.	145TS = ((2.00108) + ((85) + 45IN(-LND/R) + LND)) + D**2+LAD*D*2.*	***2*LAD*D*2**	001030	
36		101010101			001040	
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100			9. 11 60 70 5		00100	
	•				001100	
		#PITE (6, 196)			001110	
		40175 (6.142)			001130	
105	•	CALL	CALL AXIALCLAD. LAD. MACH. ABOR. ALPHA. PN. CA)		001140	
		CALL XCPBTT6	XCPHTTCALPHB.LAMDA. MACH.AR.D.S. XCPET)		001150	
			= (LND+LAD-CP/D)+ XCPST+CR/D		001100	
		CALL YOPPOUR	CALL YOUR CLADS IND STACH ALPHA XCPB >		001180	
110		J. IHGIGOTAL	JFCOPTPHI .FG. 13 GO TO 10		001190	
		CALL CATTOR	CALL CATTER PHA . LANDA . MACH . AR . CNT)		001200	
		CALL ACPTTOA	XCPTT(ALPHA.LAMDA.MACH.AP.XCPT)		001210	
		TF (ALOHA .GT.44.)			001220	
		. nc = 144				

	PROGRAM MAIN 74/	74/74 OPT=1 FTB 4-2*74355	.61.27/76 89.19.	19.19.
115	CALL CHTP	CMTPHICHACH AR OLANDA . D . S . ALPHA . PMI . CR. ALE . CMI	001240	
		SETTCLAMBAOMACHAAP ALPHAOPHIOSODOIBT)	001250	
		MCPTBECHACH AROLANDADOSOCR ALPHAOPHIORCPTB10KCP1820	001260	
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***	- 110011	TOTAL		
150	50 10 16		001300	
	300 MRITERS,2	URITTER. 204) ALPMA, CHE, XCPB, CMT, XCPT, CA	001310	
			001320	
:	16 xCP81 = 1	MODEL = CONFORCE + 2. CONTROL MAINTON MICHIEL + INTERCEDITION	-	
125	1.6131116.01	UNITED STORY ALPHANCING ACPOINT AND TO THE BOACPIEST OF THE STATE OF THE SACPIEST		
	30 ALPHA = ALPHA	ALPHA + DELAF	001360	
	-	FIALPHA .67. ALF23 60 TO 1	001370	
	KOUNT = KOUNT		001300	
130	IFCKOUNT	IF (MOUNT . EG. 50 . AND. OPTPHI . EG. 03 GO TO 4	001390	
	UNITE CALLETT	IPINII otto to militabile	001420	
	WRITE (6, 101)	101) ALPMA	001430	
135	WRITE(6,105)		001440	
	UR17E(6,102)	102)	001450	
	URITE(6,103)	103)	001460	
	URITE (6,104)	1940	001470	
	WRITE(6,105)	105)	001480	
140	KIT = KIT + 1		001490	
	IFCKIT-EG	F(K ToF0. 3) KIT = 0	001500	
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			001550	
		144 - 96 =	001560	
		CNTPHICMACHOAR, LANDA, D. S. ALPHA, PHII, CP. ALE, CNTBII	001570	
	CALL CNTP	CNTPHICMACH.AR.LAMDA.D.S.ALPHA.PHIZ.CR.ALE.CNT82)	001580	
150		PHICHACH.AR.LANDA.D.S.ALPHA.PHIS.CR.ALE.CNTB31	001590	
		CHTPHICHACH-AR-LANDA-D-S-ALPHA-PHI4-CR.ALE-CHTB4)	001600	
		ACPTERCHECH SECTEMBER OF SOCIAL PRESENT LONG PLOIS SCHILLS	001610	
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155		XCPTER (MACHARA LANDA DO SOCRO ALPHA PHIA CXCPTU CXCPTLA)	001640	
		TCPTE (LAMDA.PHII.ALPHA.MACH.S.D.CR.YCPTI)	001650	
		TCPTS FLAMDA . PMI2 . ALPHA . MACH . S . D . CR . YCPT2)	001660	
		ACPTION CLASS OF THE SECTION OF CO. O. C.	001670	
160	CALL 1911	TOTAL AND AS CASE ALPHAS PAIRS OF TOTAL AND TO	001690	
	-	IF (ALPHA.GT. 90.) 60 TO 35	001700	
	XCTL3=LAD		001710	
	XCTLZ=LAD		001/20	
***	XC11551A1		001100	
163	XCTU15LAC	XCIL+=LAC+LNO-CR/O + XCFIL+=CR/O	001750	
	XCTU2=LAT		001760	
	XCTU3=LAL	٠	001770	
-	XCTU4=LAC	XCTU4=La0+LND-CP/D + XCPTJ4+CR/D	001786	
170	50 10 36	50 TO 36	001/90	

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		X+67-3-3X	002150	
	106	196 FORMATCH! ALPHA 1 ISOLATED COMPONENTS	002160	
		ICUSATION.	002170	
	107	int I CNB I XCPB I CNI I XCP	CNT(B) 1002180	
210		YCPTCP) I C	005190	
	142		002200	
	100	A THOUT	101002220	
	110	F08*ATC1H	1.1002230	
215	111	FESHATTEL	002240	
		110	. 002250	
	112	FOF MITCH 1 141L ASPECT RATIO = F5.2	002260	
			002270	
-	113	113 FORMATTITH TAIL TAPER RATIO = **F5.2.	002280	
550				
	•11	119 FUTERITIES INTER LACE SEELY ANDLE - PATSOCAT DESKEED	602310	
	115	109 MATCH TAIL ROOT CHORD= F6.3.	1002320	
			002330	
552	116	114 FORMATETH I NOTE LENGTH ZOF 6.7. CAL.	1 002340	
			002350	
	117	117 FORMATCH I AFTER BODY LENGTH = F6.5. CAL.	1002360	
			002370	

	PROGRAM MAIN	11/16		PT=1 FTM 4-2+74355	04/21/18	04/21/16 09.19.28.
	150	150 FORMATCIN	:	BODY DIAMETER = **F5.2.*	002380	
230	151	11.) 151 FORMATCIH	:	TAIL SEMI-SPAN(INCLUDING BODY) =+.F5.2++	902390	
	118	11+1 118 FORMATCIH		RETHOLDS NUMBER =**F13.2.* 1*)	002420	
	119	19 FORMATCIH			1 - 1 0 0 2 4 3 0	
235	120	FORMATCIN	::	CNB = 80DY ALONE NORMAL FORCE COEFFICIENT	1-1002450	
	122		:	KCPH= BODY ALONE CENTER OF PRESSURE	1.1002460	
	121		:	CAT = TAIL ALONE NORMAL FONCE COEFFICIENT	1 - 1002 480	
	124	TORKA TORK	: :	CATERIA TAILLIN PRESENCE OF BODY) NORMAL FORCE	1-1002490	
0 6 7	126		:	COEFFICIENT	1.1002500	
	127		:		1.1002510	
	128	FORMATCIH	:	CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED	I - 1002520	
	161		:	AFT FROM ROOT CHOPD LEADING EDGE)	10002330	
245	129		:	YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANNISE	04500001	
	130			COUTER OF PRESSURE/TAIL SEMI-SPAR CERCLOGING	1 . 1 0 0 2 5 6 0	
	162	TO THE STATE OF		CONTRACTOR OF PRESSURE OF BOOK PLUS TAIL	1.1002570	
	151			CONFIGURATION (CAL. FROM NOSE)	1.1002580	
000	111			CHIER-TIS NORMAL FORCE COEFFICIENT OF BOOY	1.1002590	
000	134			PLUS TAIL CONFIGURATION	1.1002600	
	135			CA = AXIAL FORCE COEFFICIENT	1.1002610	
	140	FORMAT(141)			002520	
	141	FORMATCING)	10		005450	
255	200		16.33		002640	
	201		0.3		000000	
	202		0.3	FORMAT (4F 10.3.F13.2.12.12)	002670	
	203		12.0		002680	
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592	904	400 5104			002750	
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### ### ##############################		THIS SUBFOUTINE CALCULATES TAIL NORMAL FORCE COEFFICIENT IN	302780 302790	
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The control of the		01144 10364 4	002830	
## ## ## ## ## ## ## ## ## ## ## ## ##		LAMBA = TAIL TAPER RATIO	002840	
### ### ### ##########################		C = FOOT DIAMETER	002860	
### ### ##############################		ALPHA = ANGLE OF ATTACK (DEGREES)	002870	
Color		PHI = BOLL ANGLE (DEGREES)	002880	
CONTROLLER TO THE FORCE CORFF. IN PRESENTS OF CYLIN. BOOV TO THE CONTROLL OF T		ALE = LEADING EDGE ANGLE (DEGREES)	005200	
######################################		CATP = TAIL NORMAL FORCE COEFF. IN PRESENTS OF CYLIN. 800Y	002910	
PERL LMND. WARCH. WICH FOR (13) FREPLICA).  OTHER (13) FREW (15) FREW (15) FREPLICA).  FREPLICA STRIPE (13) FREW (15) FREW (15) FREPLICA).  FREPLICA STRIPE (13) FREW (15) FREW		***************************************	062930	
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### PER FORMACT   1   1   1   1   1   1   1   1   1			002990	
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			10 TO	004400	
			SIES MACH SANDS SOU SEES MACH SON	004670	
25 CONTINUE 25 CONTINUE 27 CONTINUE 28 CONTINUE 38 CONTINUE 39 CONTINUE 39 CONTINUE 30 CONTINUE 40 CON	25 CONTINUE  25 CONTINUE  26 CONTINUE  1 FIGS. **LE** WACH. **AND**1.5.*2** **GE** MACH) GC TO 30  1 FIGS. **LE** WACH. **AND**1.5.*2** **GE** MACH) GO TO 40  1 FIGS. **LE** WACH. **AND**1.5.*2** **MCH) GO TO 50  26 MAIT(6.5.00)  26 MAIT(6.5.00)  27 MAIT(6.5.00)  28 MAIT(6.5.00)  30 IF(ALPH **GE** **O**) GO TO 60  29 CALL LONGERPREPEREPERS** **RIPPAR**3*LAMOA** FAPLC**3*IX*IY*1)  40 MAIT(6.5.00)  50 TO	16(1.2	LT. PACH SAND-1-75 -GT- MACHS GO IN 230	004680	
25 CONTINUE 1 FOR 1.6.7 * 06.7 to 600 1 FOR 1.6.7 * 1.2 * 06.8 * Mach) 60 TO 30 1 FOR 1.6.7 * 1.2 * MACH * AAND* 3.0 * 06.8 * Mach) 60 TO 40 1 FOR 1.2 * 1.7 * MACH * AAND* 3.0 * 06.8 * Mach) 60 TO 50 2 WATT (6.000 ) 2 WATT (6.000 ) 3 OF TO 40 4 OF TO 40	25 CONTINUE 1 FOR 1.6.7 * DE. AND. 1.2 * GE. MACH) GC TO 30 1 FOLIS. * LE. WACH *AND. 3.2 * GE. MACH) GD TO 40 1 FOLIS. * LE. WACH *AND. 3.0 * GE. MACH) GD TO 50 2 B 917 (6.5.00) 2 B 917 (6.5.00) 3 G FGRMAT(* FFROF 3 FGRMAT(* FFROM 4 FGRMAT(* F	26 04 05		004690	
25 CONTINUT  26 CONTINUT  27 CONTINUT  28 CONTINUT  28 CONTINUT  29 CONTINUT  20 CONTINUT  20 CONTINUT  20 CONTINUT  20 CONTINUT  30 CONTINUT  310 CONTINUT  40 C	25 CONTINUE  26 CONTINUE  1 FIGURATE - WACH - AND - 112 - 6E. WACH) 60 TO 30  1 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  1 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  2 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  3 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  3 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  3 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  3 FIGURATE - LE. WACH - AND - 112 - 6E. WACH) 60 TO 50  3 FIGURATE - LE. WACH - AND - 112 - 6E. WACH - EEALET - 9. WACH - 8. WACH -	20 01		00100	
				004400	
		27	T. an. 1 CO TO 600	0.710	
			1.2 GF #4CH) GO TO 30		
FF.1.2.   LT.   MACH	FF.1.2.   LT.   MACH		ווי לבו האותה דיי כי האותה עם דס 40	004 150	
1F(1.2. LT. MACH -AAD.1.75 .CT. MACH) 00 10 30  26 4811 (16.500)  500 FRANT (16.500)  30 IF (ALPHA .CT. 20.) 60 TO 60  31 FALPHA .CT. 20.) 60 TO 60  32 FRANT (17.00)  4	15   15   15   15   15   15   15   15	16:11.75	.LE. MACH .AND.S.G .CL. MACH. CO.	004730	
26 4811164500) 500 FORMATCE FROM CONTROL OUTSIDE ALLOWARLE LIMITS*) 510 FORMATCE FROM CALL LONZE GETPERSTANCE ** PHIPERSTANCE **	26 491166500	16.1.2	-IT. MACH -AND-1-75 -6T- MACH) 6U 10 50	004740	
SOF FORMATCE FROM MACH OUTSIDE ALLOWARLE LIMITS.)  SOF FORMATCE FROM STATE POINTS AND ALLOWARLE LIMITS.)  SOF FORMATCE FROM STATE POINTS AND ALLOWARLE SEALET. STATE AND ALLOWARLE STATE AND ALL AND A	SOB FORMATCE FROM MACH OUTSIDE ALLOWARLE LIMITS.)  SOB FORMATCE FROM STATE POINTS. ARE REPARSED LANDAR REPLOSSIX. 17.1)  SOB STORMATCE FROM STATE POINTS. ARE REPARSED LANDAR REPLOSSIX. 17.1)  RIGHTLL ACT		1365	004750	
SOO FORMITTERFORM  STOP	SOD FORMSTICSTROW  STOP			001100	
30 IFGLAPHA (CT - 20.) 60 TO 60 CALL LONZ(STRPARTEPETS.AR.RIBPAR.3.LAMOA.RIBPLC.3.IX.IY.1) CALL LONZ(STRPARTEPETS.AR.RIBPAR.3.LAMOA.RIBPLC.3.IX.IY.1)  A = RIBST-RIE	30 IF (ALPHA (CT - 20.) 60 TO 60 CALL LONZ(PIPP-RIEPCT-3.AR.RIEPAR.3.LAMDA.RIBPLC.3.IX.IY.1) CALL LONZ(PIPP-RIEPCT-3.AR.RIEPAR.3.LAMDA.RIBPLC.3.IX.IY.1) R 74 C = F TPP-SIN(-7859981) A = RIEPS-RIE0 CALL LONZ(W. +KF 79.94.ALPHA.EEAL FT.9.ALE.EEALET.9.MACH.EEMACT-3.00 CALL LONZ(W. +KF 79.94.ALPHA.EEAL FT.9.ALE.EEALET.9.MACH.EEMACT-3.00 FHIPM = 90 PHIP PHIPM = 90 PHIP PHIPM = 90 PHIP PHIPM = 90 PHIP PHIPM = 50 PHIPM	200		004/00	
30 IFFALPHA .CT. 20.3 GO TO ED TEALPHA.EFALE TRPARETEPLE.3.IX.IY.1)  CERPLICATION CONTROL TO TO TO TEAL TRPARETEPLE.3.IX.IX.IY.1)  R 2 R TAKE = T TEVE SING. 785.3981)  R 2 R TEME - TO	30 IFFALPHA .CK. 20.3 GO TO BO TO TEALPHA.EFALENDA.RTBPLC.3.IX.IY.1)  FIGURE CONTROL OF TO TO TO TO TEAL THE TO TEAL THE TO TEAL TO TE			00410	
CALL LOOKZ(FTHP-RTEPTT3.AR.RTEPAR.S)LAKUARN INTLUSSINGER FF(PHILT). 46.0 TO 70 REA = FTPP-STN - 7853981)  A = RTE45-RTE0  CALL LOOKZ(H + 4FT.9-4-ALPHA.EEALFT.9.ALE.FEALET.9-MACH.BEMACT.3)-0 REA = RTE45-RTE0  CALL LOOKZ(H + 4FT.9-4-ALPHA.EEALFT.9.ALE.FEALET.9-MACH.BEMACT.3)-0 PHIPPER = 50 PHIP  PHIPPER = 50	CALL LOOKZ(FTHP-RTEPTT3.AR.RTEPAR.S)LAKUARN INTLUSORATION OF FEFTULIT. 4.5 00 10 70  RTG4 = FTP-STN - 7853981)  A = RTE45-RTE0  CALL LOOKY (H + HET49.4 ALPHA.EEALFT.9.ALE.EEALET.9.HACH.BEMACT.3).  PHIST = 45.  PHIST = 45.  PHIST = 50 PHIF  A5=(16,000.ePHIPRH-15000.*PHIPRH.CPPRIM.*2)-(PPRIM.*2)-(PPRIM.*3)/  A4=(16,0000.*PHIPRH-1200.*PHIPRH.CPPRIM.*2)-(PPRIM.*2)-(PPRIM.*3)-(A42.6.CPPRIM.*3))/  A4=(40.CPPRIM.*3)-PHIPRH-1200.*PRIM.*2)-(PPRIM.*2)-(PPRIM.*3)-(A42.CPPRIM.*3))/  A4=(40.CPPRIM.*3)-PHIPRH-1200.*PRIM.A0.*(PPRIM.*2)-PPRIM.*3)-(A42.CPPRIM.*3))/  A4=(40.CPPRIM.*3)-PHIPRH-1200.*PRIM.A0.*(PPRIM.*2)-PPRIM.*3))/  A4=(40.CPPRIM.*3)-PHIPRH-1300.*PRIM.A0.*(PPRIM.*2)-PPRIM.*3))/  A4=(40.CPPRIM.*3)-PPRIM.APPRIM.APPRIM.APPRIM.ACH.RTBPGM.3.IX.IY.1)/  CALL LOOKY (PHIPR.PRAP.APPRIM.APPHIPRAF.EEX.IX.I)/  CALL LOOKY (PHIPR.PRAP.APPHA.PHIPRAF.EEX.IX.I)/  CALL LOOKY (PHIPR.PRAP.APPHA.PHIPRAP.EEX.IX.IX.IX.IX.IX.IX.IX.IX.IX.IX.IX.IX.IX		A -61. 20.1 60 10 60	004780	
### ### ##############################	### ### ##############################		INKO (PTHP & RTEPCT - 3 - AR - RTEP AR - 3 - LAMDA - R INFLUSSIANI	004790	
# # # # # # # # # # # # # # # # # # #	# # # # # # # # # # # # # # # # # # #	רארר רי		0000	
R TRACE T FIRE SINCE TRESSENCE AND REALETAGE OF SERIET STRACTH SET OF STRACT ST	R TRACE = T TEPS SINC - TEPS STATE  CALL LOOYT (H . +6 T . 9.9.9. ALPHA.EEALFT. 9. ALE . 6 EALET. 9. HACH. 8 EMACT. 3.0  CALL LOOYT (H . +6 T . 9.9.9. ALPHA.EEALFT. 9. ALE . 6 EALET. 9. HACH. 8 EMACT. 3.0  PH 19 = 45.  PH 19 = 45.  PH 19 = 45.  PH 19 PR H = 50.4. PH 18 H = 50.00. *PH 19 PR # (PPR 18 ** 2.3) / (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.** (\$00.**	IF(PHI.	4.50	004800	
A S RIGAG-RIBO  CALL LOON; IN +66 T.9-9-8-ALPHA, EEAL FT.9-ALE , 6E CALET. 9-WACH, 8E CACT. COUNTY  TY 17 17 17 17  TY 17 17 17  TY 17 17 17  TY 17 17 17  THO THE	A S RIGAG-RIBO  CALL LOON IN +66 T 9-9-ALPHA, EEAL F 1.9-ALE • FEALET • 9-WACH, BEMACT • 3.0  • TX4 T * 17.1 )  PHIS = 45.  PHIS = 50 FHI  PPRIN = 50 FHI  PPRIN = 50 FHI  PRIN = 50 FHI  A S (16,000 • FHIPFH • 1200 • PHIPFH • CPRIM • 2) / (*00 • (*00 • 6)  A S (16,000 • FHIPFH • • 2) • PHIPFH • 2) • (PPRIM • 2) • (PPRIM • 3) / (*00 • 6)  A S (16,000 • FHIPFH • 2) • PHIPFH • 2) • (PPRIM • 2) • (PPRIM • 3) • (*00 • 6)  A S (16,000 • FHIPFH • 2) • PRIM • PHIPFH • 40. • (PPRIM • 2) • PPRIM • 3) • (*00 • 6)  A S (10,000 • FHIPFH • 0114 532)  B C IF (MELG • ED • 1) 60 TU 00  ICALL CONTINCE LPHA • LAWDA • MACH • AP • CUT)  CALL CONTINCE CO		TTep-51N(-18539H1)	004810	
CALL LOONI (4-6) - 6-6-11  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (74 17-72)  - (	CALL LOOY 1 (4) + 6 F 1 + 9 + 9 + 1 + 1 + 9 + 1 + 1 + 9 + 1 + 1			004820	
- TX   TY = 17 - 17 - 17 - 17 - 17 - 17 - 17 - 17	- TX   TY = 17 - 17 - 17 - 17 - 17 - 17 - 17 - 17	200	COLT SEE T. 9. 51 PHA. FE AL FT. 9. ALE . BE ALET. 9. MACH . BEHALI . 9.	2000	
**************************************	**************************************	כארו רח		00400	
PHIP = 45.  PHIP = 45.  PHIP = 45.  PHIP = 50 PHIF  PPAIN = 50 PHIF  A3=(15.00.0.ePIIPRH-15.00.*PHIPRM-2+400.*PHIPRM-3)/(400.*(400.*  A3=(15.00.0.ePIIPRH-15.00.*PHIPRM-12.00.*PHIPRM-6)/(PPRIM-6)/  A4= (40.* (PPIIM-7)/PPIIM-3)/  A4= (40.* (PPIIM-7)/PPIIM-3)/  PHIP = 110.* PPIIM-3)/(400.*(400.*PPIIM-6)/PPIIM-6)/  A15 = 8THO - A43 + 8 A4  60 TO 80  If (MFLAG - FG - 1) 60 TO 90  If (MFLAG - FG - 1) 60 TO 90  If (MFLAG - FG - 1) 60 TO 90  If (MFLAG - FG - 1) 60 TO 10  CONTINUE ALPHA-LAMDA-MACH-AP.CNT)  60 CALL CNTT ALPHA-LAMDA-MACH-AP.CNT)  60 CALL LONZ (RTB-PHIPTALAM-PHIPTALAM-PHIPTALAM-MACH-RTBPGM-3*IX*IY*I)  60 CALL LONZ (RTB-PHIPTALAM-PHIPTALAM-PHIPTALAM-MACH-RTBPGM-3*IX*IY*I)	PHIP = 46.  PHIP = 46.  PHIP = 50PHIP  PPAIN = 50PHIP  A3=(15.00.00.*PHIPR*-15.00.*PHIPR**-2.+400.*PHIPR**-3)/(400.*(400.*)  A3=(15.00.00.*PHIPR*-15.00.*PHIPR**-2.+400.*PHIPR**-3)/(400.*)  A4=(40.*(40.*)*PHIPR*-12.00.*PHIPR**-2)-(PPRIM**-2)-(PPRIM**-3)*(A4.*)  A4=(40.*(40.*)*PHIPR*-12.00.*PHIPR**-2)-(PPRIM**-3)*(A4.*)  A4=(40.*(40.*)*PHIPR*-12.00.*PRIM**-2)+(PPRIM**-2)-(PPRIM**-3)*(A4.*)  A4=(40.*(40.*)*PHIPR**-3)/(400.*(400.*)*PRIM**-2)+(PPRIM**-3)*(A1.*)  A4=(40.*(40.*)*PHIPR**-12.00.*PRIM**-2)+(PPRIM**-3)*(A1.*)  A4=(40.*(40.*)*PHIPR**-12.00.*PRIM**-2)+(PPRIM**-3)*(A1.*)  A4=(40.*(40.*)*PHIPR**-12.00.*PRIM**-2)*(A1.*)  A4=(40.*(40.*)*PHIPR**-12.00.*PRIM**-2)*(A1.*)  A4=(40.*(40.*)*PHIPR**-2)*(A1.*)  A4=(40.*(40.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)  A4=(40.*(40.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*)*(A1.*	I * I x • I X • I	7.11	004840	
PHIPSM = 90FHI  PHIPSM = 90FHI  A15150000.*******************************	PHIPSM = 50FHI  PPHIPSM = 50FHI  A3:(16000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**10000.**10000.**10000.**1000.**10000.**10000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**1000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**100000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**10000.**100000.**10000.**10000.**10000.**10000.**100000.**100000.**1000000.**100000.**100000.**100000.**10000.**10000.**10000.**10000.**1000	" 6110	•	004850	
PPAIN = 90.— PHIF  A1:(150000.*PHIPPM-15000.*PHIPPM*2)+400.*PHIPPM*3)/(400.*(4000.*  A1:(1500000.*PHIPPM-15000.*PHIPPM*2)  *PRIFACE.*(FPRIM.*2)*PPRIM*3)  *PHIPPM*2)*(FPRIM.*2)*(FPRIM.*3)*(  A1: (40.*(FPRIM.*3)*FHIPM*1200.*PHIPM*2)*(FPRIM.*2)*(FPRIM.*3)*(  A1: (40.*(FPRIM.*3)*(A10.*(A10.*(A10.*PRIM.*2)*(FPRIM.*2)*(FPRIM.*3)*(  A1: (40.*(FPRIM.*3)*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*(A10.*	PPAIN = 90 PHIF  A15:150000.**PHIPPM-15000.**PHIPPRM***3)/(400.**(400.**)  **PAIN - 1.***PHIPPM-15000.**PHIPPRM***3)/(400.**)  **PHIPPM***3)**PHIPPM**1200.**PHIPPRM***2)-(PPRIM**2)-(PPRIM**3)**C  **PHIPPM***3)**CHOO***CA00.**PHIM***2)-(PPRIM**2)-(PPRIM**3)**COORTING***3)/(400.**CA00.**PRIM**2)+(PPRIM**3)**COORTING***SIMPM***3)/(400.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**CA00.**PRIM***3)/(400.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**CA00.**	Medino	1144-666	004860	
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A42 (40.* (FPE IM**3)*PHIPRM-1200.*PHIPRM**2)*(PHIPRM**3)*40.*  **PHIPRM**3)*(PHIPR**3)*(FMIRCHIPRM**2)*(FPE IM**2)*(PHIPRM**3)*40.*  **PRIPRM**51)*(FMICO.*(400.*(400.*PE IM**2)*(FPE IM**2)*PPRIM**3))  **TG = FR = F	442 (40.* (FPE IM**3)*PHIPRM-1200.*PHIPRM**2)*(PHIPRM**3)*40.*  **PHIPRM***3)*(**O**1200.*PFIM**2)*(**PFIM**2)*(**PHIPRM**3)*40.*  **PHIPRM***3)*(**O**100.*(**400.*PFIM**2)*(**PFIM**2)*PPRIM**3))  **THE THE THE THE THE THE THE THE THE THE	4-MI 400.	4C++ (PPR IM++2)+PPR IM++312	004890	
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76 FF = RIFG + A+A3 + E +A4  60 TO PO  76 FF PO PO PO  80 IF (JELAG - E2 - 1) FO TO 90  80 IF (JELAG - E2 - 1) FO TO 10  110 CONTINUE CONTINUE - LAMBA-MACH-APP-CNT)  CALL COTT = RIE-CNT  RETURN FOR PROPER FOR STANDA-MACH-APP-RACH-RIEPGH-3 - IX -	76 FF = RIFG + A+A3 + E +A4  60 TO PO  76 FF PO PO  10 CONTINCE -C3 - 1) FO TO 90  110 CONTINCE CATT ALPHA-LAMBA-WACH+AR-CNT)  CALL CONTINCE REPORTED FOR 14 + ALPHA-RTEP FOAD 14 + WACH+RTEP GM-3 * IX*IY*1)  60 CALL LOOK (REP-RTEP FOT POT 14 + ALPHA-RTEP FOAD 14 + WACH+RTEP FOAD 17 * IX*IY*1)  60 CALL LOOK (REP-RTEP FOT POT 14 + ALPHA-RTEP FOAD 14 + WACH+RTEP FOAD 17 * IX*IY*1)		100 1 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	004920	
76 FT = RTP-SIN(PHI0174532)  80 TO FT = RTP-SIN(PHI0174532)  80 FF = RTP-SIN(PHI0174532)  80 FF = RTP-SIN(PHI0174532)  80 CONTINUE  CALL CONTINUE  REPORT  REPORT  60 CALL LOAZ (RTEP-RTEPGT-14-&LPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)  60 CALL LOAZ (RTEP-RTEPGT-14-&LPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)  60 CALL LOAZ (RTEP-RTEPGT-14-&LPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)	76 FT = RTP-S.IN(PHI-0174532)  80 TO FT = RTP-S.IN(PHI-0174532)  80 IF(VELAG - CG - 1) CO TO TO  10 CONTINUE  60 CALL CATTALPHA-LAMDA-MACH-AR-CAT)  60 CALL LONZ (RTEP-RTEPGT-14-ALPHA-RTEPGA-)4-MACH-RTEPGM-3-IX-IY-1)  60 CALL LONZ (RTEP-RTEPGT-14-ALPHA-RTEPGA-)4-MACH-RTEPGM-3-IX-IY-1)  60 CALL LONZ (RTEP-RTEPGT-14-ALPHA-RTEPGA-)4-MACH-RTEPGM-3-IX-IY-1)  61 CALL LONZ (RTEP-RTEPGT-14-ALPHA-RTEPGA-)4-MACH-RTEPGM-3-IX-IY-1)		340 0 4 100		
GO TO PO FO ETC = THEPSIN(PPI).0174532) BO IFUNELAG -ER. 1) FO TO SO 110 CONTINUE CONTINUE CONTINUE CALL CNTTALPHA-LAMBA-MACH-AR-CUT) ETTISM = RIB-CNT FO CALL LONZ (RIB-RIB-GT-14-ALPHA-RIB-PGA-14-MACH-RIB-PGM-3-IX-IY-1) FO CALL LONZ (RIB-RIB-PHIPTALPHA-RIB-PGA-14-MACH-RIB-PGM-3-IX-IY-1)	60 TO 80 FEG = FITHPRESINCPTI0174532) 80 FEG = FITHPRESINCPTI0174532) 80 FEG = CONTINUE - CO. 10 TO 90 110 CONTINUE - C. 10 TO 100 110 CONTINUE - C. 10 TO 100 110 CALL CONTINUE - C. 10 TO 100 110 CALL LOOK (REP-RTEPET-14-ALPHA-RTEPEA-14-MACH-RTEPEM-3-IX-IY-1) 60 CALL LOOK (REP-RTEPET-14-ALPHA-RTEPEA-14-MACH-RTEPEM-3-IX-IY-1) 61 CALL LOOK (REP-RTEPET-LPHA-RTEPEA-1X-1X)			004420	
70 ETE = RTHP-SIN(CPIT-0174532)  80 IF (JELAG - C-9 - 1) CO TO 9TO  10 CONTINUE  CALL CATTALPHA-LAMDA-MACM-AR-CAT)  FETTIN F TRE-CAT  CATTAL C	76 FTE = RTHP+SIM(PHI**0174532)  80 IF (AFLG - EQ* 1) FO TO 90  110 CONTINUE  CALL CNTICALPHA*LAMDA*MACH*R*CNT)  CONTE = RTB-CNT  RTUPH  FO CALL LOOKI (PHPP) FPHPPT*LPHA*RTBPGA*14*MACH*RTBPGM*3*IX*IY*1)  CALL LOOKI (PHPP) FPHPPT*LPHA*RTBPGA*14*MACH*RTBPGM*3*IX*IY*1)	9 OT 05	Ca	046400	
E FEGELAG -CG- 1) FO TO 90  10 CONTINUE CONTINUE CALL CONTINUE CALL CONTINUE E RECENT  CALL CONTINUE E RECENT  RETURN FOR CALL LONG REP-REPGET-14-ALPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)  CALL LONG REP-REPGET-14-ALPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)  CALL LONG REP-REPGET-14-ALPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IY-1)	E FEGELAG -CG- 1) FO TO 90  110 CONTINUE CONTINUE CALL CONTINUE CALL LOON (REPERT PROPERTY)  60 CALL LOON (REP-RTEP GT-14-ALPHA-RTEP GA-14-MACH-RTEP GM-3-IX-IY-1)  61 CALL LOON (REP-RTEP GT-14-ALPHA-RTEP GA-14-MACH-RTEP GM-3-IX-IY-1)  62 CALL LOON (REP-RTEP FF FF PHIP FF FF PHIP AT FF		p1HP+S1N(PHI+,0174532)	004950	
	FERGING CONTINUE  IN CONTINUE  CALL CNTICALPHA-LAMDA-MACH-AR-CNT)  CAT = RTB-CNT  RT TEN CNT  CALL LOOK (RTBP-RTEPGT-14-ALPHA-RTEPGA-14-MACH-RTBPGM-3-IX-IY-1)  CALL LOOK (RTBP-RTEPGT-14-ALPHA-RTEPGA-14-MACH-RTBPGM-3-IX-IY-1)  CALL LOOK (RTBP-RTEPGT-14-ALPHA-RTEPGA-14-MACH-RTBPGM-3-IX-IY-1)		200	2000	
IF (F LAG . ER. 1) FO JO JOU 110 CONTINUE CALL CATT = RIE-CNT RETURN FOR CRIEP. RIEPGT. 14. ALPHA. RIEPGA. 14. MACH. RIEPGM. 3. IX. IY. 1) COLL LOOK 1 (PHIP. PHIP. I. PHA. PHIPAT. 6. IX. 1)	IF (FLAG .ER. 1) FO JO JOU 110 CONTINUE CALL CATT LEPPA.LAMBA.MACH.AR.CVT) CALL LOCY (REP. RTEP 6T.14.ALPHA.RTEPGA.14.MACH.RTEPGM.3.IX.IV.1) 60 CALL LOCY (RTEP. RTEP 6T.14.ALPHA.RTEPGA.14.MACH.RTEPGM.3.IX.IV.1) CALL LOCY (RTEP. RTEP FILPHA.RTEPGA.14.MACH.RTEPGA.14.CH.RTEPGM.3.IX.IV.1)	38		004400	
110 CONTINUE CALL CATTELPHA, LAMBA, MACH, AR, CUT) CATE OF FRECAIT RETURN FO CALL LONZER FEP, RTEP GT. 14, ALPHA, RTEP GA. 14, MACH, RTEP GM. 3, IX. IY. 1) FO CALL LONZER FEP, RTEP FAIPHA, RTEP GA. 14, MACH, RTEP GM. 3, IX. IY. 1) CALL LONZER FEP, RTEP FAIPHA, PHIPAT, 6, IX. 1)	110 CONTINUE CALL CNTT ALPMA-LAMDA, MACH, AR, CNT) CALL CNTT ALPMA-LAMDA, MACH, AR, AR, AR, AR, AR, AR, AR, AR, AR, AR			004970	
CALL CATTEALPMA.LAMBA.MACH.AP.CAT)  CATE = RIB.CAT  RETURN CATEP.RTEP.GT.14.ALPMA.RTEPGA.14.MACH.RTEPGM.3.IX.IY.1)  60 CALL LOOKI (PHIP.PHIPT.ALPMA.PHIPAT.66.IX.1)  CALL LOOKI (PHIP.PHIPT.ALPMA.PHIPAT.66.IX.1)	CALL CATTEALPHA.LAMDA.MACH.AR.CUT)  CATO = RTB-CNT  RETURN  RETURN  COLL LOOK: CRTEP.RTEPGT.14.ALPHA.RTEPGA.14.MACH.RTEPGM.3.IX.IY.1)  CALL LOOK: CPTPP.PFIPT.ELPHA.PHIPAT.66.IX.1)		The state of the s	004980	
CMTO = RIE-CNI RETURN 60 CALL LONZ (RIEP-RIEPGI-14-ALPHA-RIEPGA-14-MACH-RIEPGM-3-IX-IV-1) CALL LONZ (PHIP-PHIPT-ALPHA-PHIPAI+6-IX-1)	CMTC = RIE-CNI RITHEN FO CALL LOAVE (RIEP-RIEPGI-14-ALPHA-RIEPGA-14-MACH-RIEPGM-3-IX-IV-1) CALL LOANI(PHIP-PHIPT-ALPHA-PHIPAI-6-IX-1)		TITE OF DIA - LABOA WACHOAP CONTO	066400	
RETURN 60 CALL LOOKICPEP.RTEPGT.14.ALPHA.RTEPGA.14.MACH.RTEPGM.3.IX.IX.1) CALL LOOKICPIP.PHIPT.ALPHA.PHIPTT.66.IX.1)	RETURN 60 CALL LOOKI (PHEP-RTEPGT-14-ALPHA-RTEPGA-14-MACH-RTEPGM-3-IX-IX-1) CALL LOOKI (PHEP-PHEP-ALPHA-PHIPAT-6-IX-1)	1 05:00		00000	
AETUEN FO CALL LONY (RTEP-RTEPET-14-ALPHA-RTEPEA-14-MACH-RTEPEM-3-IX-IY-1) CALL LOONI(PHIP-PHIPT-ALPHA-PHIPAT-6-IX-1)	# F TOFN CRIEF - RIBFGT.14-4LPH4.RTBPG4.14-MACH-RIBPGM-3-IX-IY-1) CALL LOON ICP-IPP - RIPT-& LPH4.PHIPAT-6-IX-1) CALL LOON ICP-IPP-IPP - IPP-IPP-IPP-IPP-IPP-IX-1)	- 1147			
CALL LOOMI (PHIPP-PHIPT-ALPHA-PHIPAT+6-1X-1)	CALL LOOM (PHIPP PHIPP PHIPP PHIPP PHIPP TO 18 CALL		STATES OF ALPHALETEDS ALL MACHER TEPGMES O IN TITLE TO THE TEPGMES O IN TITLE TO THE TEPGMES OF INT TITLE TO THE TEPGMES OF INT TITLE TO THE TEPMES OF THE TEPMES O		
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41F = APHA + 10. A0=07755FFF74LF** + 1,72193E-05*ALF**3 + 6. 0164580694LF + .087604485 A1 = 4.69769F-07*ALF** + 4.22259F-05*ALF**3 + 2. * 3.6936F-09*ALF* + .991598545		995599
#3==2-07752F-F7*4F** + 1-72193F-05*4F**5 + 6. 016485 #1 = 4-67767F-07*4F**4 - 4-2229F-05*4F**5 + 2. * *3-6926F-03*4F** + .991598545		005510
*016456069-4LF + .087604485 A1 = 4.69769E-07*ALF** + 4.22299E-05*ALF** 3 + 2		02550
A1 = 4.69769E-070alFoot - 4.22299E-050alFoo3 + 2		005530
* *3.6936E-03.4LF * .981598545		045500
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CALL LOURICKTFOKTFT+US-KTHOS-11-TX-11	500	092500
RTEO = AC + A1+KTE	500	005570
IF(IFLAG .F3. 1) 50 T0 290	500	005500

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	. 15272F-05.4LF003 - 8.10606E-04.4LF002 + .092902183.4LF	000000
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		105680
	CALL LOGAL (ATB-ATBT-DS-ATBDS-11-1X-1)	02570
260	A2= -2.166116-11.4LF.06 + 1.21153E-08.4LF.05 - 2.53877E-06.4LF.09	90/500
	** F ** * * * * * * * * * * * * * * * *	027.20
		005738
	COK 2 CR TEP 2 . H TEP 21 . 12 . N ACH - R TBP 2 H - 1 Z - L A DA - N - L - L - L - L - L - L - L - L - L	005740
	= PTPD2-LAMOA	005750
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100	10 = 4.5709#F-12.4LF 6 - 2.30809E-09.4LF 4.5 + 3.96812E-07.04LF	00200
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	2.15478E-04-81F-+3 + .011664495-81F-+2 -303221946-81F	99999
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	CALL PHCC (ALPHA, MACH+DCR.PHC1)	2222
	D40 = DHC1+04D	
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		060900
	OFF OF TOO CONTRACT TO SELECT	006100
222	*POWEL*OU** PENDAN PEND	006110
		006120
	IF(48-59-1-) 60 TO 620	006130
	CALL LOOKE CTRT. RTRIT. 19.10.MACH. RTRTW. 19.4 LPMA. RTRTA-10.4 R.	006140
340		001900
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PAGE 04/27/78 09.19.41. 006180 006190 006200 006210 FTN 4.2+74355 620 876 = 875 C+4 + 8PEM+P 7.174 OPT=1 SUBROUTINE CATPHI

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	0663900=================================
	THIS SUBROUTINE CALCULATES TAIL NORMAL FORCE COEFFICIENT OF .006250
	ANGLE OF ATTACK (DEGREES)
	CH = MACH NUMBER
:	
	DIMENSION FF121(25,3,3), FP1MAC(25), FP1AR(3), FP11AM(3).
	APRIMICS.SJ.APRIMICS.APRARCSJ.
	OCNTAT(11)+SCALM(9)+CNCMAT(23)+
	) .DCDMAC(3).
	Olegon equilibroa contratora e
	0.000
	DATA (((DCDCT([9-0-67-0-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-
	***25**48**59**63**7*0**46**85**95**99*1**0**15**35**47*53**65*0006460
	****24**46**5**67**79*0***52**79**9**94*1*/
	78-1./
	DATA (DCDLAM (1941=145) / 00-05910/
	DATA ((DCNMT(I-J)+1=1+7)+J=1+3)/0.0+0.0+0.0+0.0+0.0+0.0+0.0+0.0+0.0+0.0
	*0**225**255**255**25**14*0*0*0*0**11**32**465**465**42/
	DATA (CHMLAM(I)+1=1+7)/0-+1+2+3+5+0-1+0/
	DATA (CAPRIMITE) 1-1-2-2 1-1-3 1-1-3 30 30 30 30 30 30 30 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20
	.0.,21.,23.,13.,11.,11.,11./
	(APRLAM(I) 01=105)/000025905007501.0/
	DATA (APPRAR(I)-1=1-33/-5-1-00-2-0/
	08-1-1415
	DATA(DCNTAT(1)+1=1+11)/30+431-432-433-44-435-436-437-438-439-40-006510
	008950
	DATA(SCALET(I).1=1.91/1989328687887584452296/ 006630
	ONITY CONTINUE TO THE TOTAL OF
	*,2,323,2,273,2,197,2,172,2,121,2,071,2,045,2,02,1,995,1,995,1,94,006660
	*1.919*1.869*1.818*1.793*1.768*1.717*1.667*1.641*1.616*1.591*2.727*006670
	*2.12/*2.727*2.677*2.6677*2.656*2.551*2.552.5*2.5525*2.5\$2.399*2.273*2.121*006680 *2.045*1.97*1.484*1.4843*1.414*1.742*1.742*1.742*1.423*1.443*1.443*1.443*1.443*1.444
	**591.55.46.5.46.5.45.5.45.3.884.3.283.3.131.2.854.2.955.3.005.3.005.3.005.2.8006700
	.79.2.576.2.298.2.071.1.97.1.894.1.869.1.818.1.742.1.717.1.692.1.64006710
	*1*1*616*1*591*11*566*2*98*2*98*3*056*3*207*3*182*3*805*2*929*2*809*006728 *2.498*2.881*.2.727*2.626*2**2**3**8*2*292*2*3*48**
	- 2002-041-050-042-012-02-02-04-04-03-04-04-04-04-04-04-04-04-04-04-04-04-04-
	**3.712.3.409.3.182.3.005.2.879.2.702.2.525.2.374.2,247.2.146.2.02.006750
	*1.894*11.818*11.108*11.742*11.717*11.692*11.667*11.667*2*955*2*955*2*98*3006760
	106.5 OF 1 4 116.3 411.1 501.1 61.5 654 5 157 5 574 5 575 5

SUBROUTINE CNTT	74/74 OPT=1 FTN 4-2+74355	04/27/78 09.23.25.
		790
	DATA ((FPI2T(II-J-3)-I=1-25)-J=1-53/73-005-2-75-2-75-2-2-2-121-2-071-1-99006800	008
	*6.2.955.2.594.2.158.2.2.536.2.652.2.524.2.717.1.692.1.667.2.727.2.753.2.80006810	910
0	-3-2-98-3-561-3-535-3-308-3-056-2-904-2-753-2-601-2-5-2-374-2-298-200	02950
	*.222.22.121.2.071.1.995.1.944.1.919.1.894.1.8694.1.81818.1.818.1.818.1.01.01.01.01.01.01.01.01.01.01.01.01.0	2840
	**894*1.97*2.323*3*081*3*662*3*33*3*0*2*1*55*0*1*6*1*1*2*1*1*2*1*75006850	9880
	44/1/2017242004040404040404040404040404040404040	006860
•		0.85
	**1.81.9,2.0,2.1,2.2,2.3,2.4,2.5,2.6,2.7,2.8,2.9,3.0//	0689
	DATA (FPIAR(1) -1=1-3)/-5-1-0-2-0/	0069
	DATA (FPILAM (1)-1=1-53/U-U-U-0-0-1-U-V	6910
		6920
	*.55.1.585.00000579981.1.208.1.409.1.535.1.610.1.73611.7619.1069.0	940
	**811*1.686*1.610*1.56*1.55*1.55*1.55*1.58*1.083*1.0*1.1.58*1.535*1.55600595********************************	0969
	*57*1.308*1.535*1.736*1.865*1.91*(*)*1.875*1.1.75*1.1.26*1.585*1.736*1.860108960	0969
13	**1*5851*61*11*2535*******************************	0269
	-2-11-93/7-2-013-8-0-0-2-1-8-34-11-5-8-5-1-7-11-1-8-36-1-937-1-987-2-0-38-2-0-38-2006-980	0869
		0669
	-1.7746.2.189.2.138-2.088-2.013-1.937-1-862-1.786+1.761+1.7611-1.76101-7010	7000
,	-1.761.1.786.2.55111.233.0.11.434.2.013.2.314.2.39.2.365.2.289.2.1007010	7010
06	***************************************	7020
		1050
	111-736-1-711-1-686-1-71101-736-1-082579-0-001-384-2-013-2-385-201-00-00-00-00-00-00-00-00-00-00-00-00-0	2050
	**465.2.465.2.365.42.239.2.138.2.613.1.6811.1.611.1.6101.7.1.6101.0.1.0.1.0.1.0.1.0.0.0.0.0.0.0.0.	7060
85	**736*10736/	7070
•	DATA (FPSMT(I)) I = 1919/080-910-10-10-10-10-10-10-10-10-10-10-10-10-1	7080
	***1.5*1.6*1.6*1.6*1.6*1.6*1.6*2.**  *******************************	007090
	DATA (FPSAR) (1301-103)/0314-04-05	7100
	UAINTENT TO THE TABLE TABLE TO THE TABLE TO THE TABLE TO THE TABLE TO THE TABLE TABL	7110
06	***************************************	7120
	***************************************	7130
	*1.274*1.353*1.443*1.401.1-373*1.342*1.317*1.282*1.235*1.198*1.123*1.11*1.	7150
	*1.118*1.09*1.072*1.06*1.098*1.123*1.123*1.116*1.095*1.01/3*1.01/3*1.116*1.095*1.01/3*1.01/4.04.04.04.04.04.04.04.04.04.04.04.04.04	7160
96	*025*1.002**972**959**952**921**895**871**851**85***1.128**1.093*1.05071.0	17170
	*9*1*015*1*10*1*12*2*12*2*****************	17180
	#8919U2701010102701027010707070707070707070707	17190 .
	+17.1.015.1.146.1.126.1.126.1.018.1.093.1.08.1.007.1.065.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.058.1.0	17200
	*1.027**984**949**916**891**866**848**825**825**835**858**858484*********************	17220
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* CASTG13.4.4.9.CM	CARTOLO-4-+>- CARROLOD - CART RO+) - CARTOC+) -	119511
. TAUGESOI, TAULDES	20%.	119511
· CDCT4233,CDC*4233,	11.	119521
• CBCT2(12),CBC#2	(12), TMU(1+), TMUM(1+)	119531
0414 (CNALD([]),[=[,4)/2.5,	(CNALD([], ]=1,+1/2,5,3,+3,5,+./	119541
	5811./	119550
0474 (CA4*(1),1=1,13)/1.5.	(CALETT) + 1 = 1 + 131/1 - 5 + 1 - 75 + 2 - 1 + 2 - 1 + 2 - 2 + 2 - 3 + 2 - 4 + 2 - 5 + 2 - 6 + 2 - 7 +	1135611
12.8.2.9.3./		119571
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DATA (TRUM_D(1)), 1=1,201/2.	.46611121416182122	113611
124 . +26 . +28 . + 31 . + 32 . + 34 . + 36	3841./	119621
0474 (TPUM(13,1=1,2037.56)	10.5120.6420.6629.6820.7160.7210.7360	013610
1.746 755 751 771 775	.786,,791,,794,4816,,811,,816,,821/	119641
DaTateOC*(1),1=1,231/.0	198 315 55, .6 674 638 815 875 5.	119650
94,.964,1.102,1.2,1.397	11.598,1.8,1.957,2.198,2.4,2.597,2.8,3./	1 119664
DATA (CDCT ( D) +1=1+23) /1 -206	DATACCOCTCIN : 1-1-1-239 /1 -205 -1 -211 -1 -234 -1 -279 -1 -178 -1 -498 -1 -512 -	119571
* 1.418.1.433.1.6.1.874.2.0	17,1.796,1.692,1.557,1.478,1.428,1.393,	119581
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DATA CCCCNEATCIONOSTELO	DATA (((CNEAT(1,d,()),1=1,9),d=1,4),(=1,3)/4.735.4.735.4.759.	119711
14.819,4,916,5,112,5,148,5,	.012,4.964,6.470,6.587,6.566,6.565,6	119711
26.759,6.843,6.928,6.952,6.	.892.8.887.8.855.8.976.9.896.9.215.	115721
39.289,9.301,9.253,9.169,10	19.289.9.3011.9.2558.9.169.10.277:10.277:10.2377:10.68.00.00.00.00.00.00.00.00.00.00.00.00.00	119734
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34.928.4.984.4.892.6.482.6.	.516,6.578,6.699,6.831,6.916,6.916,	119751
44.819,6.735,4.735,8.723,8	.481,9.,9.,45,9.229,9.241,9.145,9.836,	119761
718-133-14-181-14-277-14-3	98.10.518.10.651.IG.831.10.94.18.94.	119771
24.639.4.627.4.699.4.795.4.	.817,4.771,4.352,4.892,4.771,6.602,	119781
96.542.6.542.6.663.6.817.6.	.711,6,627,6,55,6,578,8,651,8,675,8,6771,	. 119791
** 928.9.148.9.121.9.196.9	136.9.036.9.984,15.15.15.124,11.12010.373	3.119861
110-554-11-663-16-711-11-6	/•	019618
DATA CCCCATTCALACTOL	19.5.41.41.41.41.7.459.7.616.7.646.7.449.7.691	1.11982
10.74.9.81.0.81.0.97.0.0.	111 - 1 - 147 - 1 - 156 - 1 - 131 - 1 - 136 - 2 - 684 - 2 - 718 -	
00.706.0.366.0.366.0.366.0.360.0.360.0	601-3402603461400400140160400430400430404144	
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79.414.9.8414.9.544.9.445.1	111.1.1.168.1.192.1.115.2.172.2.781.2.768	4.1144
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SUBROUTINE CNBOD	CN800	10176	0PT=1 FTM 4-2+74355	•74355	04/27/78	04/27/78 09.24.56.
*			01 GRIJ + 14 - 0 - 14 / 14 - 0 - 14 / 14 / 14 / 14 / 14 / 14 / 14 / 14		919500	
:		RETURN			010510	
	20 16	F CHACH-LT.1	IF CHACH-LT.1.5) 60 TO 96		010520	
,	11.0 0.11	ALL 100831C	110 CALL LOOKSICNA, CNAT, 13,4 "MACH, CNAM, 13, LAD, CNALA, 4, LND, CNALD, 4,	.CMALD.4.	010530	
	.11	61xe1Ye12e1)			010548	
120	19	60 10 100			010558	
	30 05	39 CHAI=CNA			010560	
	11	IFLAG=0			010570	
	-	MACHEL.S			010586	
	7	JFL46=1			010590	
52	9	60 70 110			010666	
	13 04	40 CNA2=CNA			010616	
		MACH = MACHT			010620	
	7	JFLAG=0			010630	
	3	1.4=C442-1C*	Cha=Cua2-(Cra2-Challetta-5-PaCH)/.3		010640	
130	99	60 70 50			010650	
	11 06	IFLAG = 1			010660	
		MACHTERACH			010670	
		PACH = 1.2			010680	
	1	50 TO 16			010690	
135	75 A	75 ASALPHA.PAS			010700	
	5	NESSINCE	CNE=51N(2.01)0000(4/2.)00000*U0(SP/SPFF)0(SIN(A))002		01010	
	œ	RETURN			010720	
		240			010730	

HIS SUPPOUTINE CALCULATES BOTY ALONE CENTER OF PRESSURE	6.65100 6.65100 6.65100 7.59200 19.001 10.001 11.5011 11.5011 11.5011	THIS SUPPOUTINE CITCULATES RODY ALONE CENTER OF PRESSURE   LUD
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877. 0111 9. 0111 1. 0111 52. 01111 57. 01111 7. 01111 1. 3. 01112 01112 01122 01122 01122	877. 0111 951. 0111 32. 0111. 7. 0111. 7. 0111. 0111. 1. 3. 0112. 0112. 0112. 0112.	DATA (((VOTE (1.) 1.1 - 1.7) 1.5 = 1.5   V = 1.5   V = 852 - 802 - 2   1.2 97 + 3.7   V = 1.5   V = 1.5   V = 1.5   V = 852 - 2   RD2 - 2   V = 4.7   V = 1.7   V = 1.5   V = 1.
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1.3	, , , , , , , , , , , , , , , , , , ,	### ### ##############################
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1.3.00000000000000000000000000000000000	1.3	DATA (COTTAIN) = 1.77/1.5-1.75.2.25.25.25.25.3.5.4.5/  DATA (COTTAIN) = 1.47/4.6.48.10.6/  DATA (COTTAIN) = 1.47/4.6.48.10.6/  LATA (COTTAIN) = 1.48/4.6.48.10.6/  LATA (COTTA
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	1 . 3 .	DITA (MOTELACI):
3.	1.3	DITA (XDTZLKT): 1-1,27/2-05-3-54-10./  PATA COLLING: 1-1,27/2-03-3-54.  1-15-2-201-2-35/4-251-25-15-3-17-11-091-07  2-287-2-35/4-254-251-25-1-57-11-091-07  1-4-1-4-5-1-5-1-5-1-7-1-5-2-2-2-3-4-2-5-2-5-3-2-1-1  UFLAC = C
1. 3. 3. 4. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.		DATA (CELLATION 1-1-37/2-0-5-5-4.7  1-1502012051-27/7-1501-5713812411109107  2-26720520520520520520520520
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1.3	1.167.2017.17.13.17.15.17.15.4.157.138.174.11.091.07 2.227.285.285.286.286.286.286.286.286.286.286.286.286
1.3	1.3	2.257.254. 2.257.254. DATA (DELXM(1).1=1.21).//6.695274.258.283.283.285.286. JELMG = 0 LD = LNC+LAB ISAGE-67. 1.2) 60 TO 10 129 CALL LOGYKOLYGTI+C+4.MACH+XOTIM+5.LAB.XOTILA+4.LND,XO 36 CALL LOGYKOLYGTI+C+4.MACH+XOTIM+5.LAB.XOTILA+4.LND,XO JF(JELM5.EG.1) 60 TO 10 JF(JELM5.EG.1) 60 TO 10
1.3		CACTARRAY  DATA  11.4.1.46E.XX(1).1=1.23)./f69GP011.855902952.11  SEAR = CACTARRAY  LD = LAN-LAD  IE WELH-67. 1.29 60 TO 16  129 GAL SOCIACO-XCOTI-6.4.XCH-XOTIP-5.LAD.XOTILA-4.LND.XO  FOR IT FOR EC. 10  17 FIFT LAGE CO. 10 OF TO 10  18 FIFT LAGE CO. 10 OF TO 10  18 FIFT LAGE CO. 10 OF TO 10
DATA (OELXW(I),I=1,23)/46.695.401.855.902.952.1.11.1.2.1.3.01120  JELAG = 0  LELAG = 0  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720	DATA (DELXMID).1=1,233/-(1-675801855902952.11.11.2.1.3.01190 JELAC = (-4.0.1.5.1.6.1.716.22.2.2.4.2.596.2.794.2.9.3.7.1.1.2.1.3.011200 JELAC = (-4.0.1.0.0.0.0.1.716.22.2.2.2.4.2.596.2.794.2.9.3.7.1.1.2.1.3.011200 LD = (-4.0.1.0.0.0.0.1.2.1.2.1.2.1.0.1.0.1.0.1.0	DATA (DELXM(1),1=1,23)/,f.e695P01855902952.1]  11.41.455.1.551.611.711.6.22.2.2.4.6.596.2.796.2.9.3]  12.40.= 0.  12.40.450.= 0.  12.40.450.= 0.  12.40.450.450.= 0.  12.40.450.450.1
11.4.1.465.1.5.1.6.1.7.1.1.6.2.2.2.2.4.2.596.2.952.1.1.1.1.2.1.3.011200 JELMG = [	11.4.1.465.1.5.1.6.1.7.1.6.29.2.2.4.2.556.2.798.2.1.1.1.1.2.1.3.011200  JELAG = C  LNC-LAG  IENTROPES - 1.00 TO 10  17.50 CALL LOOKING XGT1.6.4.XACH.XOT1P.5.LIG.XOT1LA.4.LND.XOT1LN.3. 011210  37 X = X0-4.AG  18 KIELAG.EG.1) GO TO 10  18 KIELAG.EG.1) GO TO 10  19 KIELAG.EG.1) GO TO 100  11 KIELAG.EG.1) GO TO 100  11 LOOKING XGT1.6.4.XACH.XOT1P.5.LIG.XOT1LA.4.LND.XOT1LN.3. 011260  11 LOOKING XGT1.6.10 GO TO 100	11.4.1.465.1.5.1.6.1.7.1.6.2.2.2.2.4.2.55902952.1.1  JELMG = [
JELAG = C	JELAG = 0 JELAG = 0 JELAG = 10 LD = LAN-LAD JE CALL LOCKICKG-VCTI-C-4-VACH-VOTIM-5-LAD-VOTILA-4-LND-VCTILW-3- JE CALL LOCKICKG-VCTI-C-4-VACH-VOTIM-5-LAD-VOTILA-4-LND-VCTILW-3- JE CELL LOCKICKG-VCTI-C-4-VACH-VOTIM-5-LAD-VOTILA-4-LND-VCTILW-3- JE CELL LOCKICKG-VCTI-C-4-VACH-VOTIM-5-LAD-VOTILA-4-LND-VCTILW-3- JE CELLAG-EC-1) GO TO 100 JE	JELAG = C 18 LAG = C LD = LAG-LED LD = LAG-LED 120 CALL LOGASKO XGOTTO 1C 120 CALL LOGASKO XGOTTO CAGANACH XOTTP * SALAD * YOTTLA * ALND * XO 17 TY 12 13 C 18 FOR LOGASKO CONTO TO 100 18 FOR LAG ECCT 10 COTTO 100 18 FOR LAG ECCT 10 COTTO 100
		128 544-57-1-27-60 TO 16 128 544-1405-57-1-27-60 TO 16 128 544-1405-57-1-4-4-7-4-7-4-7-4-7-4-7-4-7-4-7-4-7-4-
		LD = LNT-LDD 129 CALL LOCKXCO1.70 60 TO 10 1X.17.12.1) 30 X0 = X04-10 30 X0 = X04-10 1F(LDC-1) GO TO 10 1F(JELAS-EC-1) GO TO 10 1F(JELAS-EC-1) GO TO 10
		IF (MACH.ST. 1.2) 60 TO 10  129 CALL LOGGIKO.KGT1.6.4.W4CH.KOT1P.5.LAD.XOT1LA.4.LND.KO  1X-1Y-1Z-13  37 XO = XV - LAD  1F(IFLAG.EG.1) GO TO 10  1F(JFLAG.EG.1) GO TO 10
200000	110000	120 CALL LOGK31X 0. X 0. 17 1. X 0. 17 1. X 0. 12 1. X 0. X
10000	00000	1X-1Y-1Z-1)
0000	2000	30 x0 = x04-Lab 16 (16 Lab -6-1) x0 TO 100 16 (16 Lab -60-1) 00 TO 10
1111	000	37 XO = XO - X - LAC 1 XO = XO - X - LAC 1 F(JFLACE CO - 1) CO TO 10
GO TO 100	60 TO 180	60 TO 18
00 TO 110	00 10 110	60 TO 11
12 130	00 10 110	11 01 00
	011300	

PAGE

-31

PAGÉ 04/27/78 09.25.22. 011880 FTN 4.2+74355 SUBROUTINE KCP500 74/74 CPT=1 CNC

115

••••	SUBROUTINE IETT(LAMDA,MACH,AR,ALPHA,PHI,S,D,18T)	011890
v		.011910
<b>.</b> .	THIS SUBROUTINE CALCULATES RODY NORMAL CARRYOVER FORCE COEFF.	•011920
	4111	•011930
٠٠		011940
0	= 1411	0061100
U	ANGLE	-0111990
U	"	10001100
v	= TAIL	111990
·		-012000
	BCOY	•012010
		•012020
	Print Charles and the same of	+012030
	* 139AS*MACHT. 11. 12. 12. 18. 19. 18. 12. 18. 19. 18. 18. 18. 18. 18. 18. 18. 18. 18. 18	012040
	*191*	
	NOI	012070
	* ISBT(5,3), IBTM(5), IBTAR(3),	012080
	* FCART(6) FCATT(6) .	012090
	* ICPAST(2), ICBADB(2),	012100
	PARMITOSONOFAMAC(S) PREMER(S) .	01210
		0112120
	* IABAST(2) - IAPDB(2) -	012121
	TFERREID OFFER CIDS	01212
	* TF208(13) TF092(13)	01216
	TERMES TERMECHES.	01210
	* TI2EAS(11) • TI2ELM(11) •	012170
	* TF1DF(13),TF0B1(13),	012180
	DATA (((TDIET(1.J*K).I=1.6).J=1.3).K=1.3)/00.018106405A84	
	11.639.0021193329.649.1.117.000231092995577680.	
	2.015068214086460.0180811672964460.20.071.	012220
	3-1492563040013043139218271-0013051109155-012230	.012230
	4.2050.00.0150.0430.099.1370.122/	012240
	OATA (DIBTAF(1)+1=1+6)/0-+5-+10-+15-+20-+25-/	012250
	DATA (DISTLM(1)+1=1+3)/0++5+1-/	012260
	DATA (DISTARII) (1=103)/05010020/	012270
	DATA ((1981(10.1))   110.5)   1210.1)   1.464	012210
		012280
	/CI+++0-0-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	015290
		012300
		012310
		012320
		012330
		012340
	DATA (ICEADE(I).1=1.2)/.35/	012380
	DATA ((FARMT(10.0)) [= 10.5) 0.0=10.3) /10.780 10.6680 10.44940 10.00.00.00.00.00.00.00.00.00.00.00.00.0	01216
	12.02.02.03.03.03.03.03.03.0	01210
	DATA (FAMAC(1) 0   = 1 0 5) / 0 5 0 0 8 0 0 0 1 0 0 1 0 1	2000
	OATA (FAMAP(1) 121 3)/551 02.	01210
	OBTA (FARRICI) 0 = 10113/205970201180107140103110110114401	01200
	111.	2000
	DATA (FFAR(1).1=1-11)/-46756467867160801-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	016710
	11.55.2./	012420
	0171 (1101011111111111111111111111111111	
	UAIA (IAEAST(I).IEI.2)/1.5.1./	

2 2 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	012460 012460 01240 01240 01240 01240 01250 012510 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520 012520	FIN 4.2+74.555 04/27/78 09.26.41.
		3.86(1).1=1.10)/.013.176366504645756632906. 012460 3.8(1).1=1.10)/.5655856.11.86.1.364.1.511.669.1.835.012480 208(1).1=1.12)/1
Date (172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172   172	Out of the first   Out of the	*1=1*13)/****317**333**35**368**365**4**424**39***39***35***424**459***35***45***45***459***45
Unit (TT   Det   1)   1   1   1   1   1   1   1   1	1.344. (1970-11). 1313/11\$7\$16\$75\$66\$75\$66\$75.002500 1.444. (1970-11). 1313/11\$7\$16\$75\$66\$65\$66\$66\$75.002500 1.444. (1970-11). 1313/11\$13\$14\$15\$15\$15\$65\$66\$66\$15\$15	TICELECTION   1 = 113/2 - 12   1   1   1   1   1   1   1   1   1
	1.40	DATA (TFIDE(1)*151-151/1***89**788**659**656**56**56**456**419**012580 012590 DATA (TFIDE***54-5/16***545/
FLACE = 0	First	5333349367384418435.
### 5 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		
### = PIYER   PARTIES   PA	### ### ### ##########################	1.46 = 9
DE = DAS IF (AACH, -(1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	DE = DV4  IF (FRACE, GT - 1.3) GO TO 10  SO CALL LOOKITE LASS - LAST - L	= P1/180.
		2005 = D/F
80 CELL LOOKIGEAS IZERSI TOP 20 CELL LOOKIGEAS IZERSI TOP IZER 10 20 CELL LOOKIGEAS FEAFINE 10 10 10 20 CELL LOOKIGEAS FEAFINE 10 10 10 20 CELL LOOKIGEAS FEAFINE 10 10 10 10 10 270 CELL LOOKIGEAS FEAFINE 10 10 10 10 10 10 10 10 10 10 10 10 10	36 CELL LOOK 11 FEAS. 10 TO 10 20 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 27 20 10 20 20 20 20 20 20 20 20 20 20 20 20 20	
CALL LOOK; [FARE TARK TARK TARK TARK TARK TARK TARK TARK	CALL LOOKIFAKE, FART, 1877 117, 17, 17, 17, 17, 17, 17, 17, 17,	CALL LOOKI (1/645, 1/6/57 C
I = I	FAM = FAM = FAM = AND   FAM = AND   FAM = C.   SAM = FAM = FAM = FAM = FAM = FAM   AND	
	14. 1 1848.6	
CALL LOOKICEAS ICREAS ICREAS PRINTS (17.1)  CALL LOOKICEAS CARTARA (ETAR, 18.1)  LC = 1 Characteas (Cartara (17.1)  LC = 1 Characteas (Cartara (17.1)  A = A LPHARA (17.1)  If A LPHARA (17.1)  If A LPHARA (17.1)  A = A L	CALL LOGAT (ICEASTACATIVETY 5.48.16TAR.3.IX.1Y.1)  OLZ 20  IC = 1CEASTACK FCART.48.FCATT.5.1X.1)  OLZ 20  IC = 1CEASTACK FCART.48.FCATT.5.1X.1)  OLZ 20  IC = 1CEASTACK FCART.48.FCATT.5.1X.1)  OLZ 20  IF A PHARACA  SO TO SO  A DETIC = 10.589.12-39.R69.IC.(130.271.IC-13.286.IB).A.(2.244.IB-5.58612.86)  OLZ 20  A DETIC = 10.589.IC-39.R69.IC.(130.271.IC-13.286.IB).A.(2.244.IB-5.58612.86)  OLZ 30  A DETIC = 10.589.IC-39.R69.IC.(130.271.IC-13.286.IB).A.(2.244.IB-5.58612.86)  OLZ 30  OLZ	
C	C =   C   C   C   C   C   C   C   C	
# = Alphaeard   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   012210   01221	### A LEMP4.RED    FIGLEPH	
IF FIGURE   170   18 + 2   40   01   40   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   18   01   01	14 (LLPHA .67. 130.) 60 TO 40  18 10 12 830  19 10 10 10 10 10 10 10 10 10 10 10 10 10	
\$\( \text{16} \) \\ \text{16} \\ \text{16} \\ \text{16} \\ \text{17} \\ \text{16} \	012840  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  40 16 10 56  50 16 56  50 16 56  50 16 56  50 16 56  50 16 56  50 17 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56  50 18 56	JF ( ALPH B. 67 - 130 - ) 60 TO 40 JF TO 60 TO 40 012830
40 1610 = 10.592-12-39-F69-IC-(30-271-IC-13-286-IB).A-(2-244-IB-5-596012850  50 1670 = 10.592-12-39-F69-IC-(30-271-IC-13-286-IB).A-(2-244-IB-5-596012850  50 17 56	*** 16 10 50 0 10 28 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 50 0 10 5	00000
50   FFPH   .01 .01 .00 .00 .00 .00 .00 .00 .00 .00	50   FFFPH . ST. 20.) (0 TO 55   C. 20.0   C.	
F = PH.J-P.D.  55 F = (PH.J-P.D.)  56 T = (PH.D.)  57 T = (PH.D.)  58 F = (PH.D.)  58 F = (PH.D.)  59 T = (PH.D.)  50 T = (PH.	P = PH:-PAG 50 TO 50 TO	50 IFFRMI of 1 30.1 C C C C C C C C C C C C C C C C C C C
55 P = (PHI-76.)*PAD  56 JF (ALFHA .01.*9AD  CALL LOOKS (OTET * TOIST* 6.3 * ALPHA* DIETAF* 6. LAMDA* DIBTLM*3.AR* DIETAR* 012950  13.14417* 17.17  60 CALL LOOKS (OTET * TOIST* 6.2 * 25.* DIETAF* 6. LAMDA* DIBTLM*3.AR* DIETAR* 012950  61 CALL LOOKS (OTET * TOIST* 6.2 * 25.* DIETAF* 012950  62 CALL LOOKS (OTET * TOIST* 6.2 * 25.* DIETAF* 6. LAMDA* DIETH*3.AR* DIETAR* 012950  70 IST = 1570* DIET* (-16.*P** 27(PI/2.)** 2** 32.*P** 3/(PI/2.)** 3** 15.*P** 012950  *** (PI/2.)** 3** 15.*P** 012990	55 P = (PHI-06.)-PAD  56 IF (ALCHA 60.)-PAD  56 IF (ALCHA 60.)-PAD  56 IF (ALCHA 60.)-PAD  56 IF (ALCHA 60.)-PAD  57 INTERPRETATION OF TOTAL 6.3 A LACHA 4 DIBTAF-6 A LAMDA 5 DIBTAM 5 A R 5 DIBTAM 6 DI 29 40  60 TO 70 CALL LOOKS (U) ET + TOTAT-6.3 - 25 - 5 DIBTAF-6 A LAMDA 5 DIBTAM 5 A R 5 DIBTAM 6 DI 29 40  60 TO 70 TOTAT 5 - 10 TOTAT 6 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	n = PHI-PA.0
56 IF CALCHER . GT . 25.) GG TO 60  CALL LONGSCOTET . TCIET. 6.3. ALPHA.DIETAF. 6. LAMOA.DIETLM.3. AR.DIETAR.DI230  3.5. (AT. 17.2.1)  60 CALL LONGSCOTET. TCIET. 6.3. ALPHA.DIETAF. 6. LAMOA.DIETLM.3. AR.DIETAR.DI230  60 CALL LONGSCOTET. TCIET. 6.3. A.S.S.S. BIETAF. 6. LAMOA.DIETLM.3. AR.DIETAR.DI290  70 IET = 1570-518T*(-16.*P**?/(PI/2.)************************************	56 IFFALCHE 07.25.) GO TO 60  CALL LOOKSGOIET TOIST.6.3.4LPHA.DIBTAF.6.1LAMDA.DIBTLM.3.4R.DIBTAR.012940  0. TO 70	50 TO 56
CALL LOGKS OFFIT TO SECTION OF SE	CALL LOGKS OTET * TO IST * 6. 3. ALPHA, DI RTE* 6. LAMDA, DIRTLM, 3. AR, DIRTAR, DI 2930  *** TAKIN' 12.1)  ** TAKIN' 12.1)  *** TAKIN' 12	FCALPHE CT 35
\$\langle \text{17.12.1}\$ 60 10 70 70 60 CALL LOOKSTOIET. TEIST. 6.5.2.25.0 IBTAF. 6. LAMDA. DIBTLM. 3. AR. DIBTAF. 012950 60 CALL LOOKSTOIET. TEIST. 6.5.2.25.0 IBTAF. 6. LAMDA. 016 TLM. 3. AR. 01817R. 012970 70 18T = 18T0.018T. (-16P**2/(P1/2.)**2*32.*P**3/(P1/2.)**3-15D***********************************	*** (KAIT**12*1)  *** (KAIT**12*1)  *** (CALL LOG*2) (D1291***********************************	87 - TO FOT - C
60 CELL LORSIGIET, TDIRT, 6.3,25.018TAF, 6.1AMDA, DISTLM, 3,4R, DIBTAR, 012960 -3,17,17,12,13 70 IST = ISTO+DIRT*(-16.*P**2/(P1/2.)**2*32.*P**5/(P1/2.)**3-15.*D**01890	60 CELL LOGYZ(DIET.TDIET.6.3.25.0DIETAF.6.LAMDA.OIGTLM.3.AR.OIBTAR. 012960 70 IET = ISTO-DIET16P2/(PI/2.)**2*32P**3/(PI/2.)**3-16.*P***0187AR. 012900 7 (PI/2.)****0187AR. 012900 7 (PI/2.)****0187AR. 012900	SO TO TO TO TO THE DESCRIPTION OF THE PROPERTY OF THE PROPERTY IS ARE DETERMINED ON TO THE PROPERTY OF THE PRO
70 15T = 15T0+018T+(-16.*P**2/(P1/2.)**2*5**D**5/(P1/2.)**3*AR**018TAR* 012950 */(P1/2.)**4)	7.0 1547 = 1510-01547. 7.0 1547 = 1510-01547.(-16.+Pe-2/(P1/2.)**2*32**P**3/(P1/2.)**3-15.*P**0151AR. 012990 7.(P1/2.)***9. 1) 60 T0 80	60 CALL LOOK 3 (0) FAT - FT PAT - FT PA
*/(P1/2.) *** () ******************************	**(101/2-);***(10 10 10 10 10 10 10 10 10 10 10 10 10 1	70 15T = 15TO-015-12
	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	*/(p1/2,)***) 01290

200	SUBROUTINE IBIT	181	74/74 007=1	FT# 4.2-74355	04/27/10	04/27/70 09.26.41.	PAGE
•			ACTUAL				
		:	16.46 - 4		013030		
					17304		
					013050		
					090610		
					013010		
			06 01 00 TO		013080		
			1872 = 187		061210		
			MACH = MACHT		911110		
			18T = 1872-(2.0-MACH).(1872-1811)/.7		013120		
25			RETURN		013130		
		:	IF CRACH . GE. 2.) GO TO 90		013100		
			IFLAG = 1		013156		
			MACHT = MACH		013160		
			MACH = 1.3		013170		
30			60 TO 30		013180		
		90	CALL LOOKI (TIBAS.TIIBAS.LAMDA.TIIBLM.2.1X.1)		013190		
			CALL LOOK 1 (F 108 . TF 108 . DB . TF 081 . 13 . IX . 1)		013200		
			11 = 118AS-F108		013210		
			CALL LOOKIST28AS.TI28AS.LAMDA.TI28LM.11.1x.1)		013220		
35			CALL LOOKI (F2MeTF2MeMACHeTF2MACHe2eIxel)		013230		
					01 1200		
					013250		
					113260		
			13 = .5.F3AR		011270		
			IF CALPHA .61. 90.) 60 TO 105		013280		
			IBTO = II-SINCALPHA-RADI		0113900		
			60 70 110		013300		
		105	1F ( ALPHA .GT. 115.) GO TO 120		013310		
			1810 = 11-(11-12) . SQRT((ALPHA-90.)/25.)		013320		
+2			GO TO 110		013330		
		120	IB10 = -19.325+13+11.926+12+(15.816+13-8.382+12)+(ALPHA+RAD)	2) - (ALPHA-RAD)	013340		
		•	**(1.46*12-5.076*13)*(ALPHA*RAD)**2		013350		
		110	110 187 = 1870		013360		
			IF (JFLAG .EQ. 1) 60 TO 100		013370		
20			RETURN		013380		
		50	WRITE(6,500)		013390		
		200	FORMATCIH MACH NUMBER OUTSIDE ALLOWABLE LIMITS	15.1	013400		
			RETURN		013410		
			CNO		013420		

.26.45.	
:	
04/27/78 09.26.45.	013430
FTN 4-2+74355	
	SUBBOUTINE XCPBTT(ALPHA, LAMDA, MACH, AR, D. S. XCPBT) 013430
0PT=1	CP811(A
11/11	BROUTINE
XCPBTT	ns .
UBROUTINE XCPGTT 74/74 OPT=1	00

2		-013450
DENIS SUBMO	THIS SUBMOUTINE CALCULATES TAIL-TO-BOOT CARRY OVER MURRAL FUNCE	-013470
רבשונע מו	T DOOR T	-013480
	= ANGLE OF ATTACH (DEGS.)	.013490
LANDA	TAPER RATIO	•013500
		•013510
		•013520
	= 800Y DIAMETER	•013530
8	TAIL SEMI-SPANCINCLUDING BODY)	•013540
XCPT	= TAIL TO BODY CARRY-OVER NORMAL FORCE CENTER OF	013550
	PRESSURE/TAIL ROOT CHORD. MEASURED FROM.	•013560
	ROOT CHORD LEADING EDGE - AFT (ALPHA 0 TO 90 DEG)	•013570
	ROOT CHORD TRAILING EDGE - FUD CALPHA 90 TO 180 DEG1013580	101358
·		•013590
	***************************************	***013600
REAL LAMBA, MACH	MACH	013610
DIMENSION	DIMENSION TCP4(8,4,3), TBAR(8), TDB(4), TLAM(3),	013620
	TCP3(8,4,3),TCP2(8,4,3),TCP1(8,4,3)	
DATA CCCTC	4(1, Jok), 1=1,81,J=1,41,4K=1,31/0,,184,,369,,426,,50.5	
1.51.510.1.	1.55.02414458272378851879.036968195.1.135.	_
21.291,1.43	21.291.11.433.1.546.0638.1.106.1.475.1.801.2.113.2.355.2.582.0	
3.261 456.	3.261,.456,.489,.5,.5,.5,.5,.5,00,,394,,672,.806,.894,.978,1.056,	
41-128,0	41.128,0.,.572,.95,1.2,1.4,1.6,1.79,1.97,0.,.956,1.478,1.883,2.256,	
52.578.2.86	52.578,2.867.3.196.0.9.333.494,.59.50.59.50.500.0.5390.7720.8830	013690
6.994.1.089	6.994.1.089.1.189.1.278.0789.1.122.1.4.1.661.1.911.2.144.2.361	. 013700
70.01.161.1	70.1.161,1.783,2.322,2.78,3.26,3.65,4.03/	013/10
DATA CTBAR	DATA (TBAR(I)+I=1+8)/0+1-+2+93+4++5-05+0+7+/	0112120
	(TDB(II)   = 1,47/026/	013740
DATA CILAR	8	013750
DATA CICTA	7 4	10.0
2-6195-966-1	1.314.318.4.37/4.63.4.646.4.646.63.374.63.54.666.6666.6566.6566.33.426.482.6498.	
3-5-0-5-5-5	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
4.666.9666	4.6664.6654.6664.6664.6664.34.6664.8664.6664.6664.	013790
50 354 4	50.,.354.,449,492,.5,.5,.5,.5,.6,.6,.6,.639,.666,.666,.666,.666	013800
6.666.0.00	6.666.0656656666656656668666666.0666666666666666.	.0138
7.666 666 666	1991	013820
DATA CECTO	DATA (((TCF2([+J+K),1=1+B),J=1)4),H=1,3)/O1640.2180.240.250.25013830	.0138
1.2525.0.	1.2525.012917189195195195195.0.195.01115168174.013840	•0138
2 - 174 174 •	2.174174174.0.19.19.136156163163163163.016300169223.	013850
3.24425	50.250.250.250.00.140.1940.2150.2210.2210.22100.22100.012	•
4.183204.	4.183.004.214.214.214.214.2140.4.1164.1754.1964.2034.2034.2034.2034	0138/0
20.001.000	JUNEAR DOVERNIA DE SERVICIO DE LA CONTRACTOR DEL CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACT	011880
7 25 35 35 35	14-2124-6224-62444-624-624-6241-64-1274-62134-62334-644	013900
TATA CCTT	0.000.000.000.000.000.000.000.000.000.	013910
1.265.255.	2255 2.25 x 2.25 x 2.25 x 2.5 x 45 9 x 4 3 6 x 4 12	
2-473469-	473.4469.469.469.50.509.5110.5110.5110.5110.5110	013930
3.25.25.2	3270.250.250.250.250.250.250.2940.3160.3270.3270.3270.32	7.0139
4.3274.254	4.3274.254.3054.33554.33584.3584.3519.3610.3610.251.4.255.3164.3534.3710 013950	0139
5.378378.	.378,.378,.378,.378,.378,0162,.219,.233,.246,.251,.251,.251,0.016	2.013960
6.219233.	.219233246251251251.0.162219233246251251.	01397
7.251.01	251.61622192332462512511251/	01 19R
		00/610

SUBROUTINE XCPBTT	XCP811	11.71	0PT=1 FTN 4.2-74355	04/27/78	09.26.45.
	840	4A0 = PI/160.		014000	
	- 40	DP = 0/12.151		010010	
	16141	LFHA.GT.9	IF CALFHA.67.90.3 69 TO 18	014020	
	IF CM	ACH. GT. 1	IF (MACH-67. 1.) GG TG 20	014030	
	EF TA	= SGRT(1	BETA = SGAT(1MECH++2)	01+0+0	
	875	848 = OFTA.AR		014050	
	CALL	LOOKSCKC	CALL LOOKS EXCERS. TCP1.8.4.54R.TF.4R.0B.TDR.4.LAMDA.TLAM.3.IX.IY.		
	(1.51.				
	# V 0+	40 A = ALPHA-RAD		014080	
	910	= (2A	01F = (2.040.3)//PI/2.1003-(3.040.2)/(PI/2.1002	014090	
	XCPB	T = XCPBC	XCPBT = XCPBO+UIF+(XCPBC5)	014100	
	RETURN	88		014110	
	10 IF CM	ACH. 67. 1	IF (#ACH. 67. 1.) CO TO 30	014120	
	BETA	= SCRT(1	BETA = SCRT(1PACH0.2)	014130	
	848	BAR = BETA.AR		014140	
	כעוו	LOOKSCAC	CALL LOOMS (MCPRO. TCP2.8.4. BAR. TBAR.8. DB. TD8.4. LAMDA. TLAM.3.1X.IV.		
	112.13				
	= 4 05	A = (180 ALPHA) RAD	PHAINEAD	034170	
	910	= (2	DIF = (2.04003)/(PI/2.)003-(3.04002)/(PI/2.)002	014180	
	XCPE	T = XCPEC	XCPET = XCPEG + DIF * (XCPEG5)	014190	
	RETURN	22		014200	
	20 BETA	= SGRTCH	BETA = SCRT(MACH2-1-)	014210	
	474	PAP = SFTA.AR		014220	
	CALL	LCOKSCXC	CALL LCOM3 (XCPBO+TCP3+8+4+5AR+TBAR+8+08+TDR+4+LAMDA+TLAM+3+1X+IY+	Y. 014230	
	115011				
	1 09	00 TO 40		014250	
	SO BETA	= SGRTCH	BETA = SCRTCMACH 2-1.)	014260	
	240	BAR = RETASAR	•	014270	
	CALL	LOOKS CXC	CALL LOOKS (XCPBO, TCP4, 8, 4, BAR, TBAR, 8, DB, TDB, 4, LAMDA, TLAM, 3, IX, IY,		
	112.13	-		014290	
	60 10 50	0 20		014300	
	ON 4			014310	

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PAGE

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PAGE							
09.26.47.							
04/21/18	014890	014900	014910	014920	014930	014940	010000
FIN 4.2+74355							
097=1			TOTAL STREET,	<b>D</b>			
74/74 097=1	56 10 30	TINUE	THU = XCPTE	181 = XCP181	TINUE	URN	
ROUTINE XCP158	05	400 04	40x	X	30 00	REL	JN 3

	SUBROUTIN	SUBROUTINE YOPTS (LAMBA, PHI, ALPHA, MACH. S. D. CR. YCPT)	ACH.S.D.CK.YCPT) 014960
	THIS SURE	UTINE CALCULATES THE TATE	THIS SURPOUTINE CALCULATES THE TAIL SPANNISE CENTER OF PRESSURE - 611-990
	21914	ANGLE OF ATTACK	(056)
,	4		•
	83	1008	•015020
3	0	= GOOY DIAMETER	050510•
0	TONT		040610.
o	NOCH	* ACH	
3	PFI		090210.
U	,	= CENT-SPAN (TAIL PLUS BOOK RADIUS)	
	1001	SPANAISE	CENTER OF PRESSURE
			0015100
	0 1 14 14 14 14 14 14 14 14 14 14 14 14 1	SFAL LAWDA . MACH . XY	
	PIMENSION	TLAMPACSS.TRADECIES. IY	TLAMMA (3) . TRADA(11) . TYCPT(11, 3) . TMACH(6) . TALPHA(10) 015120
	PINENSION	TIMENSION TAYCID.6)	
	DATA CTLA	OATA (TLAMOA(1) . [=1,3)/05.1./	015140
	DETA (184	OF(1) . [ =1 . 11) / 0 . 05 . 0 . 1 . 0 .	DATA (TRADE(1) - [=1-1]) /0 - 05 - 0 - 1 - 0 - 2 - 0 - 3 - 0 - 4 - 0 - 5 - 0 - 6 - 0 - 7 - 0 - 8 - 0 - 9 - 0 - 0 1 5 1 5 0
	6687		015160
	DATACCTYC	ot([.J).[=1,11).J=1.3)/6.	
	1.31318.	.325330331425414.	1.31314.374.325330331425414402401402407401425407426015180
	2.410.436	0.4410.4850.4710.4590.455	
	1664.8		015210
	DATACTMAC	UATA(TMACH(I).1=1,61/0.8-1.2-1.4-1.651.15-5-0/	15610 (56500)
	CATACTALP	HA(1).1=1.10)/0.0.5.0.10.	0.14.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
	19.656	Pa 17 17 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	45.67
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	100 = 07CB		
	CALL PHEC	CALL PHOCEALPHA, MACH. DCR . PHC1)	015300
	Hd = DIHd	= PHC1 + 90.0	015310
	PADE = 0/	= 0/12.151	015320
	IF(PHI-51	IF CPHI-51. PHIC) 60 TO 10	
	CALL LOOK	CALL LOOK? ** Y * TKY . 10 . ALP P. E . TALP HA . 10 . MACH . TMACH . 6 . IX . IY . 13	
	CALL LOCK	2 (YCP. TYCPT.11. RADG. TRADG	.1)
	YCPT = KY	= KY•YCP	
	IF CPHI-LE	IF CPHI-LE -90.03 60 TO 15	015370
	YCPIT = YCPI	143	
	YCPT = YC	YCPT = YCPTT+((FHI-90.0)/(PHIC-90.0))**3 * (1.0-YCPTT)	0)) (1.0-YCPTT) 015590
			014510
-	10 (0011406		015420
			015430
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	Sui	BROUTINE XC	XCPTT(ALPHA-LAMDA-MACH-AR-XCPT)	48 . XCPT3	615460	
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٠,٠		7410	The same may be a		.815488	
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v		LAMBA:	1426		. 615540	
U		SACHE	FREE STREAM MACH NUMBER	UMBER	.015550	
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v		xte3x	TAIL CHORDWISE CENTER	ITER OF PRESSURE (RETURNED	.015578	
0.			VALUE)		.015580	
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,	**	MUTATION TO 183		X	009610	
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		ASK.	T(14,3,3),XCPDHC(14)	OXCPOLM (3) OXCPOAR (3)	915650	
		144	HT (14.43.F MACHM(14),	FMACHT (14.4).FMACHM(14).FMACHA(4).	015660	
		X DO	PT (21) + 00x M (21)		915678	
	0.11	TA (XCP9LMC	0.1=1.21)/60511	DATA (XCP9LM(I)+I=1+21)/6++051+-10-152++201+-252+-381+-35-+462-	015680	
	1.45	115020.55	** 64.6529.7019.7529.	8011.6521.9020.951010/	015696	
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	041	TA CCCXCPAT	I.J.K). I=1,20),J=1,3	J.K.1.33/.662662659659.	015720	
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	3.61	30.64566	1.6745756861.718	765, 836, 919, 118, 118, 199	. 615750	
		60.36539	4194394611.480	498,.517,.534,.547,.551,.561	. 015760	
	5.59	6 6 5 7 7 5		1.623,.615,.625,.637,.658,.657	. 015770	
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		20.058.05	.683683637652	**657 **662 **667 **5 81 ** 699 ** 711	. 015820	
	1016	6/108/100	1. 1920.8650.9820.471	***************************************	. 015830	
		10.578.59	.613623630537	**642**647**662**696**757**873	. 015848	
	7.0	90.51638	.373.407426446	*** 56** 471** 483** 495** 507** 517	. 015850	
	70.		.561598694775	,	015860	
		ATTACK T	i=1.201/05.,10	20.,30.,40.,50.,60.,70.,80.,90	615870	
		02110.0110	130.,140.,150.,160.	,170.,160./	015880	
	10	A CYCPALT	1.1=1,3)/05,1./		015890	
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		30.954.94	934969862863	** 852 ** 846 ** 844 ** 9 ** 908 *	015920	
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	***	1.850.19	.777.925.94.995.	.98968782978575723.	015960	
	1.3	6 695 68		0.8239.8147719.7059.649.614	. 015970	
	1.59	**584**584	563.583583935.	.934,.916,.903,.874,.849,.825,	015980	
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2000	SUBMOUTINE ACPT   147.4 OPT=1 FTM 4-2-74355	04/21/18	04/27/78 14.19.27
	12.6.2.8.3./	016210	
	DATA (XCPDLM(1)-1=1-3)/0-0-5-1-/	016040	
09	DATA (XCPDAR(I) 01=103)/05010020/	016050	
	DATA ((FMACHT(1.J)) I=1.14)		
	1345,503,589,628,645,643,643,628,-072,067,		
	201919627238255164568765564616-	-	
	3.114116116026196269372503654621616.		
65	4589549483151156163026274314314-	016100	
	530903060301029402840277/		
	DATA (FMACHM(1)) 1=1914)/660-860100102010401050108020020202040		
	12.6.2.8.3./		
	DATA (FMACHA(1) 01=104)/-50100105020/	016140	,
10	DATA (DDXCPT(1).1=1.21)/.000701302026032038.		
	104404905506065069074078082086089-		
	Z-0995-0961		
	DATA (DDXM(I) + I=1+21)/1++1+1+1+2+1+3+1+4+1=5+1+6+1+7+1+8+1+9+2++	016180	
;	12-1-2-2-2-3-2-4-2-5-2-6-2-7-2-8-2-9+3-/		
2	91 = 514159265	016200	
	140 = 717180	016210	
	CALL LOOKI (XCP90 + XCP90T - LAMDA + XCP9 LM + 21 + 1X + 1)	016220	
	IF (ALPHA-67. 90.) 60 TO 10	016230	
	CALL LODK3(XCPA, XCPAT, 20, 3, ALPHA, XCPALF, 20, LAMDA, XCPALM, 3, AR,	016240	
80	*XCPAAR+3+1X+17+12+13	016250	
	DELXCP = XCP90-XCPA	016260	
	CALL LOOK2 (FRACH - FRACHT - 14 - MACH - FRACHM - 14 - AR - FRACHA - 4 - IX - IY - I)	016270	
	XCPT = XCP90 - DELXCP+(1.+FMACH)	016280	
		016290	
65	10 CALL LUONS (YCP) BUOXCFATO 20030160 . XCPALF . 200 LAMDA . XCPALM . 30 AR.	016300	
	*XCPARKS IX IY IZ II	016310	
	CALL LOOKS (XCPD) XCPD1+3+3+M4CH +XCPDMC+14+LAMDA+XCPDLM+3+AR+	016320	
	* ACPURAGO IVO IVO IVO IVO IVO IVO IVO IVO IVO IV	016330	
00	11 THE CHAPTER 1-3 60 TO 20	016340	
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	20 CHILL LOCKING CONTON	016360	
		016910	
		016160	
66		016400	
	SI = (XP160-XCP90)/(P1*(70*/180*))	016410	
	A = ALPHAPPED	016420	
	B = 112-75928 - 81-47410A + 14-587890A2	016430	
-	C = -32.57471 + 22.32992*A - 3.61911*A**2	016440	
001	XCPT = XCPO + 8+DXCP + C+SI	016450	
	PETURN	016460	
	40 CALL LOOK 3 (XCP30, XCP41, 20, 3, 90. "XCPALF, 20, LAMDA, XCPALM, 3, AR.	016470	
	I TO TO A	016480	
50	BETTERN THE TOTAL	016490	
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# C PROPERTY OF BATTLE TO TAIL ROOT CHORD	OF ATTACH  VOMBER OF MODI DIAMETER TO TAIL ROOT CHORD  O16500  OF ROOT DIAMETER TO TAIL ROOT CHORD  O16610  O16610
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570-21-68-02-66-2-64-6-6-1-6-6-3-6-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9	7.66.504.743.62.644.1.540.02.015900 .56.80.44.74.22.644.1.540.02.015910 .56.80.44.74.22.67.41.65.01.690 19.61.04.60.19.59.11.56.04.016930 7.62.56.86.19.59.11.56.04.016930
6170-72-166-55-185-67-331-25-137-72-13 781-5-80-4-80-4-81-11-86-45-9-7-16 8197-75-176-22-86-82-145-85-8-87-38 9118-75-12-5-11-22-15-135-85-135-85-13-87-88	7.22.92.20.91.10.10.10.10.10.10.10.10.10.10.10.10.10
1160. no. 1166.117.17. ps. 119.03.198.06.203.73.20.65.198.26.  041. (CC19.72.72.02.72.72.72.72.72.72.72.72.72.72.72.72.72	13.73.20.465.198.26. 15.73.20.46.126.42.42.6.21. 15.73.20.43.21.70.42.6.11. 17.73.20.43.21.73. 17.73.20.22.62.43.42.77. 17.73.20.22.62.42.42.73.

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3626.96/ 0ATA (PCIMZA(I),1=1,19)/0.*2.55.5.*7.5,10.*12.5.15.*17.5,20.*22.*25. 1.*27.5.30.*32.5.35.*37.5,40.*42.5,55./ 0ATA (PCIMZA(I),1=1,12)/.8*1.*1.2,1.*4,1.6*1.8*2.0*2.2.*2.4*2.6*2.8*3. 13.0/ 0ATA (PCIMZO(I),1=1,3)/.5**75*1.*/ IFOCR.6E.1.) DCR=1. IFOCR.6E.1.) DCR=1. IFOCR.6E.1.) DCR=1. IFOCR.6E.1.) PCR=1. IFOCR.7.0*1.*1. IFOCR.7.0*1.*1.*1. PCIMZO*3*IX*IX*IX*IX*IX*1.*2*1.*2*12*ALPHA*PCIMZA*19*MACH*PCIMZM*12*DCR*, RETURN ENDR		2549.74.583.1.604.63.624.13.635.55.644.25.647.17.647.17.641.33.	017400	
DATA (PINZAII):=1:19/00.2.55.775:10.0:12.50.15.017.5.2022.0.22.0.25.  1.427-55.00.432-5.55.437.5.40.442.5.45./  DATA (PCINZAII):=1:10.10.10.10.10.10.10.10.10.10.10.10.2.0.10.2.2.2.2		3626.96/	017410	
1.427-5430.437-55.55.400.422.55.45./  DATA (PCIM2P(I).1=1.427/-601.01.21.401.601.892.00.2.2.2.42.66.2.80.  DATA (PCIM2D(I).1=1.437/-50.75.1./  IFOUR.666.1.) DCRE1.  IFOUR.666.1.) DCRE1.  CALL LOOKS(PHCIM2.PCIM2.15.12.ALPHA.PCIM2A.19.MACH.PCIM2M.12.DCR.  PCIM2D.3.IX.IX.IX.IX.1.0.1  RETURN  ENDE		DATA (PCIMPA(I)+I=1+19)/0+2-5+5+0+7-5+10+12-5+15++17-5-20-+22-+2	25017428	
DATA (PCIM2M(I), I=1,12)/.841.41.21.44.1.641.842.042.2.2.24.2.642.8.8.  13.07  DATA (PCIM2D(I), I=1,3)/.54.75.1.7  IFOCR.6E.1.2 DCR=1.  IFOCR.6E.1.3 DCR=1.  IFOCR.6E.1.4 DCR=1.  FOCR.6E.1.5 DCR=2.5  CALL LOOK 3(FOLTM*) PCIM2.15.12.4LPHA.PCIM2A.19.MACH.PCIM2M.12.DCR.  PCIM2D.3.IX.IX.IX.IX.12.1)  PHCI = PHCIM2/HACH**2  FUURN  FUURN		1.+27.55.30.+32.50.35.+37.5.40.+42.5.45./	017440	
•		DATA (PCIM2M(I)+I=1+12)/-8+1++1-4+1-6+1-6+1-8+2-0-2-2-2-2-4-2-6-2-1	8-017440	
DATA (PLIM2D(I),1=1,3)/.575,1./ IFOCR.EE5) DCR.1. IFOCR.EE5) DCR.2. CALL LOOK3(PHCIM2.PCIM2.)5.12.ALPHA.PCIM2A.19.MACH.PCIM2M.12.DCR. PCIM2D.3.IX.IY.12.1) PHCI = PHCIM2.MACH2 RETURN END		13.0/	017450	
IFOCR.6E.1.) DCR=1. IFOCR.4.E5) DCR=.5 CALL LOOKSTOPLN2-PCINZ-15.12.ALPHA.PCINZA.19.MACH.PCINZM.12.DCR. -PCINZD.3.IX.IX.IX.12.1) PHC1 = PHCINZ/MACH.*2 RETURN		DATA (PC1M2D(1)+1=1+3)/-5,-75,1./	017450	
IFOCR.LE5) DCR=.5 CALL LONGSCHPLAP.PCIM2.»5.12.ALPHA.PCIM2A.19.MACH.PCIM2M.12.DCR. .PCIM2D0.5.IX.F17.13. .PHCI = PHCIM2/MACH.**2 RFUGN END		IF(DCR-GE-10) DCR=10	017470	
CALL LODK3(PHCIM2.PCIM2.)5.12.ALPHA.PCIM2A.)9.MACH.PCIM2M.12.0CR.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.PCIM2.P		IF(DCR.LE5) DCR=.5		
*PCIM2D*s IX=IY=IX=I) PHCI = PHCIM2/MACH**2 RETURN END		CALL LOOKS(PHCIM2+PCIM2+15+12+ALPHA+PCIM24-19+MACH-PCIM2M-12-DCR-		
PHC1 = PHC1H2/MACH++2 RETURN END		*PC1M20*3*1X*1Y*1Z*1)		
		PHC1 = PHC1M2/MACH++2	017510	
01300		20100	017520	
			017530	

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SOURCE AND SOURCE AND SOURCE S	47.18			1				2	FTN 4-2+14355	04/21/18	14-19-37.
		SUBROUTINE	AXI	ALCLAD.	. ND	SUBROUTINE AXIAL (LAD. LND. MACH. ANDR. ALPHA. RN. CA.)	PHA . RN	.CA)		018570	
3	*****		:		:		*****		***********	****018580	
•		THIS PROGR		CALCULA	TES	THIS PROGRAM CALCULATES THE AXIAL FORCE COEFFICIENT ON THE BODY	RCE CO	EFFICIEN	NT ON THE BO	DY +018590	
•										*018600	
3			,,	LENG	LENGTH OF	F AFTER-BODY	DIVID	ED 87 80	AFTER-BODY DIVIDED BY BODY DIAMETER	*018610	
J			"	LENG	O H	LENGTH OF NOSE DIVIDED BY BODY DIAMETER	ED BY	BODY DIA	METER	*018620	
J			"	MACH	MACH NUMBER	PER				•018630	
J		ALPHA	"	ANGL	10 E	ANGLE OF ATTACK				*018640	
2				REYN	SOTO	REYNOLDS NUMBER				+018650	
٥		42		AXIA	FOR	AXIAL FORCE COEFFICIENT	ENT			•018660	
5										•018670	
		**********	:	*****			*****		************		
	_	DIMENSION 1	LAD	4).TLN	113)	DIMENSION TLAD(4).TLND(3).TMACH(12).TRN(14).TCAOCA(14).TCDB(12).	RN(14)	. TCAOCA	14), TCDB(12	018690	
	•	TCA18(8.4.3) . TMACH1(8)	1.0	ACH1 (P						018700	
•		REAL LAD. LND. MACH	0	EH						018710	
		DATACTLABCI	-	1041/6	.0.1	DATA (TLAD (1) . I=1,4)/6.0,10.0,15.0,18.0/	2			018720	
		DATA (TLND(1) 01=1050/10502050505/	•	1000	205	593.5/				018730	
		DAIALIMACHO	-	12101=	9.0	UNINCIPACHILING 1=10123/U-6000/00-8000/91-01-101-201-301-502-002-50188/40	1.00.1	.1.1.2.1	.301.502.00	2.5.018740	
	•		:							018750	
	-	THE PERSON AND A P				001-1-1-14BCH11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	10101	201037		018760	
		THE PERSON AND THE PE	1	1477	100	VEH ALTER A TENE	. 3E Ub.	1.554.06.	1.856.06.2.5	SE0 018770	
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		1.51.00.515.	5	2-0-63		739-0-795-0-6	112.0.	117.0.81	7.0.928.0.9	010040	
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		1.265.0.322	-	24.0.3		127-0-396-0	456.0		63.0.518.0	210-01000	
	3	0.520,0.528		9.0.06	2.0	10-520.00-528-0-590.0-652-0-664-0-667-0-751-0-751-0-766-0-798-0-865-014880	751.0	751.0.7	66.0 - 798.0	365-01880	
	3.5	0.900,00,000	.0.	10.0.01	7.00	912,0.932,0.	959.1	004.1.0	39.1.054.1.	59.018890	
	30	0.329,0.329	.0.3	32.0.33	.0.4	50-32990.32990.33290.33490.35490.40390.42690.44880.55590.52890.52890	426.0	448.0.5	25.0.528.0.	528,018900	
	•	.530560	009	9.609.	1200	5.530.550600609612788.0.793.0.793.0.793.0.883.0.879.00.8810	793.0	793.0.8	83.0.870.0.1	387,018910	
	*	0.885,0.925	.0.	27.0.92	7.0.	\$0.885,0.925,0.927,0.927,0.932,0.982,1.019,1.011,1.016/	019.1	0111010	16/	018920	
	•	CALL LOOKI	000	TCDB. H	CH.1	CALL LOOK1 (CDB, TCDB, MACH, TMACH, 12, IX, 1)	-			018930	
		ALPHAP = (9	100	.03.51	16 5 1	ALPHAP = (9.0/7.0)+SIN((ALPHA-90.0)/57.2957)+57.2957	1.2957	1.57.295	1	018940	
	-	IF (MACH. 67.1.3) 60 TO 70	-	60 10	70					018950	
		ALL LOOK !	2043	ATCADO	AORA	CALL LOOK I (CAOCA+TCAOCA+RN+TRN+1++1X+1)	•				
	-	CIVITATIONS		. ICALO		CALL LUURS (CAID+) CAID+8+++ARCH+  FACHI+8+  AD+  LAD+4+  ND+1 ND+3+ X+	SOLAD	TLAD	LND+TLND+3+		
		CA1 = (CA18-(0.04*) AD))*CADCA	- (0	041140	47.0	470				018780	
		CA0 = CA1 + CDB	COB							01870	
	, 1	IF (ALPHA.LT.20.0) 60 TO 10	T.20	.03 60	101					019010	
	-		.96.	3 60 10	50					019020	
		CABAR = -1.	3	1.42857	VH.	= -1.3 + 1.42857 * (MACH-0.6)				019030	
	•	FMA = -0.8		9 CALPY	14/57	FFMA = -0.844889+(ALPHA/57.2957) + 1.92007+(ALPHA/57.2957)**	2007	ALPHA/5	2	- 019040	
		1.445868.	1	4/57-29	- 12	1.445868*(ALPHA/57.2957)**3 + 0.360182*(ALPHA/57.2957)***	20 CALF	HA/57.2			
	. :	O T T T C C C C C C C C C C C C C C C C		7	2	0 0111/014 014 014 014 014 014 014 014 014 014	4236	ALPHAIS		• 019060	
	,	60 TO 30	-	131.6693	:	GO TO 30	O CALP	4/57.29	2730043	019070	
	10 6	FFMA = -51M(4) PHA/57_29571002	1	HA157.2	9671	•••				00000	
	30 0	CA = CAO +FFMA	FRA			•				001010	
		60 70 40								014110	
	20 C	API = - 12.	9217	-9.1867	AM).	20 CAPI # -(2.9217-9.1867*(MACH)+14.0023*(MACH)**2-8.7943*(MACH)**3+	CHACH	1.2-8-7	943+ ( MACH) ++		
	\$2	\$2.4985.(MACH) **4-0.2658.(MACH) ** 5)	:	4-0-265	8	ACH30053					
										****	

11.10	666	91117110	 -
IF (alpha, 6f. 160.) 60 TO 15	70 15	01910	
CA = CAO-(CAO-CAPI).SIN(ALPHAP/57,2957)	N(ALPHAP/57.2957)	019150	
50 TO 40		019160	
15 CONTINUE		019170	
CA = CAPI		019180	
60 10 40		019190	
70 IFIALPHA-67.90.1 60 TO 50	90	019200	
CAN = (-0.0008 + 0.1501	CAW =(-0.0008 + 0.1501+(MACH/LND) + 0.3641+(MACH/LND)++2 + 0.0928+019210	8.019210	
SCHACH/LND3 0.0409	\$ CMACH/LND) 3 - 0-0409 - CMACH/LND) 4 - 0-004 - CMACH/LND) 5) / (0-7 - 019220	. 019220	
SMACH**2)		019230	
CALL CSF (RN. MACH.CF)		019240	
CASF = (4.0/5.0)*CF*AUOR	*00	019250	
CAD = CAU . CASF +CDB		019260	
CA = CA0		619270	
60 70 43		019280	
50 IF (ALPHA-GE. 160.) 60 TO 60	10 60	019290	
CAPI = -(2,9217-9,1867	CAPI = -(2-9217-9-1867-(MACH)-14-0023-(MACH)2-8-7943-(MACH)3+	_	
12.4985.(MACH) ** 4-0.2658. (MACH) ** 5)	8 - CHACH3 5)		
CA = CAO-(CAO-CAPI).SIN(ALPHAP/57.2957)	N(ALPHAP/57.2957)	019320	
60 TG 40			
60 CAPI = -(2.9217-9.1867	60 CAPI = - (2.9217-9.1867*(MACH)*14.0023*(MACH)**2-8.7943*(MACH)**3+		
\$2.4985.(MACH) ** 4-0.2658.(MACH) ** 51	8 - (MACH) 5)	019350	
CA = CAPI		019360	
40 CONTINUE		019370	
RFTURN		019380	
Can.		001010	

SUBROUTINE CSF	CSF	11/11		0PT=1					FIE 4.	FTN 4.2-74355	•	1/12/10	00/27/78 10.19.
		SUBROUTINE CSF(RN.MACH.CF)	CSF	RN. NA	CH.CF.							119400	
		010610000000000000000000000000000000000	:	:	•	:		•		:	:	019410	
		THIS PROGRAM CALCULATES THE SKIN FRICTION COEFFICIENT ON THE BODY	H CAL	CULAT	ES THE	SKIN	FRICTIO	N COEF	TCIENT	- T	E 800Y	-019420	
•		**	"	REY	RETNOLDS NUMBER	UMBER						-019440	
		MACH	"	MAC	MACH NUMBER							-019450	
	0	*		SKI	FRICI	TION C	SKIN FRICTION COEFFICIENT	ENT				-019460	
												-019470	
		, , , , , , , , , , , , , , , , , , ,	:::	•		•	•••••				:	019480	
01		REAL MACHALAM	14									019490	
		6 = 1.4										019500	
		LAM = 1.0/	SCRTC	15.07	16-1-	D. HAC	= 1.0/SGRT((2.0/((G-1.0).MACH2)).1.0)	1.0				019510	
		CF1 = 0.07	.::	0/RM.	.23.1	.17/0	= 0.074.(1.0/RN2)*1.0/(1.0*(0.9*(6-1.0)/2.0)*MACH**2)**.44	(6-1-0)	1/2.03	MACHO	23	4 019520	
		FCF1 = (A	SINCL	AM3/L	IM) - 1 - (	J/SORT	11.0.1	6-1.0)/	72.03.H	ACH 2	101.24	= (ASIN(LAM)/LAM)-1.0/SGRT(1.0+((6-1.0)/2.0)*MACH**2)*(.242/019530	
	-	\$5GRT(CF1))-AL0610(CF1-RN)+1.26+(AL0610(1.+((6-1.)/2.)+MACH++2))	-4106	10 CCF	-RND-	1.26.1	ALOG100	1.0166	-1.1/2.	J.HACH		019540	
		CF2 = CF1 + 0.00001	. 0.0	1000								019550	
		FCF2 = (A	SINCL	AP1/L	LH) -1 .(	1/SORT	11.0.11	6-1.0)	72.03.H	ACH 2	101.24	= (ASIN(LAM)/LAM)*1.0/SORT(1.0+((G-1.0)/2.0)+MACH**2)+(.242/019560	
	-	LSGRT (CF2))-ALOG10(CF2*RN)+1.26*(ALOG10(1.+((G-1.)/2.)*MACH**2))	-AL06	10 CF	2.RNJ+	1.26.1	AL 06100	1.0166-	-1.1/2.	D. MACH		019570	
		1 = 1										019580	
20	10	OCFOOF = ((CF2-CF1)/(FCF2-FCF1))	CF2-	CF13/	IFCF 2-1	CF 113						019590	
		CF3 = CF2 - DCF0DF*FCF2	- DCF	00F .F	CF2							019600	
		IF (FCF2-LT-0.0) 60 TO 15	.0.0.	1 09	0 15							019610	
		CF3 = CF1 - DCF00F+FCF1	- DCF	90 PF	: 11							019620	
	15											019630	
52		FCF3 = (A	SINCL	AM)/L	M) - 1 - (	J/SORT	11.0.11	6-1.0)/	72.03.H	ACH 2	10 (.24	= (ASIN(LAH)/LAH)-1.0/SQRT(1.0+((G-1.0)/2.0)-HACH++2)+(.242/019640	
			-AL06	10 CCF	S-RNJ+	1.26.1	AL06100	1.0116-	-1.1/2.	J. MACH		019650	
		IF(ABS(FCF3).LE.0.000001) GO TO 20	33.66	.0.00	1001	50 10	20					019660	
		CF1 = CF2										019670	
		FCF1 = FCF2	2									019680	
30		CF2 = CF3										019690	
		FCF2 = FCF3	3									019700	
		IF(N.67.50.0) 60 TO 30	9 (0.	0 10	30							019710	
		GO TO 10										019720	
	20	CF = CF3										019730	
35		60 TO 50										019740	
	30											019750	
	35		. T	E. ITE	THE . ITERATION HAS		GONE THROUGH SO CYCLES+)	ROUGH	SO CYCL	[5.1		019760	
	20											019770	
		PETURN										019760	
0.		ONS										019790	

Su	SURROUTINE LOOK!	L00K1	14/14	0PT=1	=	FTN 4.2+74355	04/27/18	04/27/78 14.19.53.	
		15	UBROUTINE LOC	SUBROUTINE LOOKI (F.FT.X.XT.NX.IX.MULT)			017540		
			***********	001/10222222222222222222222222222222222	******	***************************************	**017550		
		C ONF	-DIMENSIONAL	DNF-DIMENSIONAL TABLE LOOKUP ROUTINE (+ = RETURNED VALUES)	TURNED	VALUESI	017560		
		J. )	**	= FTCK)			017570		
			-	FUNCTION TABLE FTENRS			017580		
		2	~	NO. OF ROUS IN FT-TABLE			017590		
		2	-	NO. OF COLUMNS IN FT-TABLE			017600		
		×	-	WORKING VALUE OF INDEPENDENT VARIABLE	ARIABLE		017610		
		×		INDEPENDENT VARIABLE TABLE			017620		
		2	*	DIMENSION OF XT TABLE			017630		
		1.	×	X INDEX ON PRIVIOUS LOOKUP (UPDATED ON EACH CALL)	UPDATED	ON EACH CALLS			
			MULT	=0. USE PREVIOUS X					
		0					017660		
		******		***************************************			***************************************		
		0	DIMENSION FT(1) . XT(1)	1) • xT(1)			017680		
		-	IF CHULT-132,1,2	• 2			017690		
		1 C	ALL INDEXCX.	CALL INDEXIXOXTONXOIXOKEEPORXI			017700		
		2 F	2 F=FT(IX)				017710		
			IF (KEEP-1)3,4,3	.3			017720		
		3 6	3 F=(FT(1X+1)-F)+RX+F	J.RX.F			017730		
		*	RETURN				017740		
		u	END				017750		

	SUBROUTINE	SUBROUTINE LOOK3 (F.FT. NR. NC. X. XT. NX. Y. YT. NY. Z. ZT. NZ. IX. IX. IX. MULT)017760	12.MULT301776
•		C*************************************	111111111111111111111111111111111111111
u	THREE-DIMENS	THREE-DIMENSIONAL TABLE LOGNUP ROUTINE (* = RETURNED VALUES)	
v		=FTCX+Y+Z) (RETURNEC VALUR)	017790
v	FT	FUNCTION TABLE FTCARONCOMPS	017800
v	N.	NO. OF ROWS IN FT-TABLE	017810
v	NC	NO. OF COLUMNS JN FT-TABLE	017820
3	X.Y.2	MORKING VALUES OF INDEPENDENT VARIABLES	017830
v	XT.YT.ZT	INDEPENDENT VARIABLE TABLES	017840
u	NX . WY . NZ	DIMENSION OF XT, YT, ZT TABLES	017850
v	*1x,11,12	X.Y.Z INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALD17860	EACH CALO1786
v	MULT	=0. USE PREVIOUS X.Y.Z	017870
U		=1. LOOK UP NEU X.Y.2	017880
	************	22	18811881
	DIMENSION	DIMENSION FT(1),xT(1),YT(1),ZT(1)	017900
	1F(#ULT-1)2,1,2	12.1.2	017910
	1 CALL INDEX	1 CALL INDEX (2 . 2T . NZ . 1Z . KEEP . R 2)	01792
	I = 1+(12-1)+NR+NC	-1) • NP • NC	017930
	II = I+NP+NC	340	017940
	2 CALL LOOK2	2 CALL LOOK2 (F .FT(1) .NR.X.XT.NX.Y.YT.NY.IX.IX.IY.MULT)	017950
	1F (KEEP-1)3.4.3	13.4.3	017960
	3 CALL LOOK2	3 CALL LODK2 (F2.FT(II) .NR.X.XT.NX.Y.Y.YT.NY.IX.IY.1)	01797
	F=(F2-F)*R2+F	13.6	017980
	4 RETURN		011990
	GNS		018000

SUBROUTINE LOOKS	L00K2	14/74	0pT=1	FTW 4.2-74355	04/21/18	04/27/78 14.19.36.
					000000	
	S	UBROUTINE L	SUBROUTINE LOOK2 (F of Tonk ox ox Tonk of of tonto Ixo I to HULL)	.IX.IV.MULIS	016320	
•				***************************************		
0	=	WO-DIMENSIC	TWO-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES)	= RETURNED VALUES)	018340	
•			=FT(X+Y)		018350	
	-		FUNCTION TABLE FT(NR.NC)		018360	
	N. N.		NO. OF ROWS IN FT-TABLE		018370	
	2		NO. OF COLUMNS IN FT-TABLE		018380	
	*	X.Y	HORKING VALUES OD INDEPENDENT VARIABLES	NT VARIABLES	018390	
•	×	X1.YT.	INDEPENDENT VARIABLE TABLES		018400	
	2	N. W.	DIMENSION OF XT. TT. TABLES		018410	
	-	1x.17	X.Y INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALLO18420	DKUP CUPDATED ON EACH	ALL018420	
	E	MULT			018430	
			=1. LOOKUP NEW X.Y		018440	
				***************************************	018450	
	0	INCISNIAN FI	DIMENSION FT(1) exT(1) eYT(1)		018460	
	1	1F (MUL T-1120102	11.2		018470	
	1 0	ALL INDEXC	CALL INDEX(YOTTONYOIYOKEEPORY)		018480	
	-	= 1+(IY-1)+KR	) • KR		018490	
	1	11 = 1+NR	*		018500	
	2 5	ALL LOOKICE	CALL LOOKISF .FTST., X. XT. NX. 1X. MULT)		018810	
	=	IF (KEEP-113.4.3	.4.3		016520	
	3 6	ALL LOOKI (	CALL LOOKI (F2.FT(II).X.XT.NX.IX.1)		018530	
	-	F=(F2-F) +RY+F	•		018540	
	- 8	RETURN			018550	
	3	END			018560	

SUBROUTINE INDEX	INDEX	10/10	OPT=1 FTN 4.2+74355	04/27/78	04/27/78 14.19.35.
	SUBI	TOUTINE 1	SUBROUTINE INDERCHONTONS INOREPORATION	018010	
	TAPLE	NOE X 1 00	C	018020	
	×		BORKING VALUE OF INDEPENDENT VARIABLE	018040	
•	TX 3		INDEPENDENT VARIABLE TABLE XTENX)	018050	
	XX 3		DIMENSION ON X-TABLE	018060	
	XI 3		INDEX OF PREVIOUS LOOKUP CUPDATED EACH CALL)	018070	
	C .KEEP			018080	
	U		=1 X.EG.XT(IX). INTERPOLATION NOT REQUIRED.	018090	
0	C .RATIO	01	INTERPOLATION RATIO	019100	
	DIMIO	DIMENSION XT(1)		. 018120	
	RAT	RATIO = 0.		018130	
	KEE	0 = d33X		01810	
51	IFC	IF (NX-1X)1,102	••	018150	
	1 1x	IX = NX-1		01810	
	2 160	JF (1X-113,304		018170	
	3 1x	IX = 1		018180	
	1 160	IF (NX-1)10.10.5	0.5	018190	
92	5 150	IF (xT(IX)-X)6.10.7	6.10.7	018200	
	6 150	IF (XTC1X+1)-X)8,9,11	x18,9,11	018210	
	7 IX	Ix = 1x-1		018220	
	141	1F(17-119.5.5	9	018230	
	8 1x	IX = 1X+1		018240	
25	IFC	IF( [x-Nx)5,10,10	6.10	018250	
	41 6	X = 1X+1		018260	
	10 KEF	KEFP = 1		018270	
	RET	RETURN		018280	
	11 PAT	X-X) = 01	PATIO = (x-xT(IX))/(XT(IX-1)-XT(IX))	018290	
30	RET	RETURM		018300	
	CAL			016310	

## Appendix B. DESCRIPTION OF SUBROUTINES AND PROGRAM LISTING

Table B-1 lists the subroutines and gives their basic function.

A detailed description of each subroutine will not be included in this report. The logic and procedures required of each included method are discussed in detail in Reference 1. The applicable section of Reference 1 for each of the Methodology Program Subroutines is listed in Table B-1.

TABLE B-1. LIST OF PROGRAM ELEMENTS

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
MAIN	of cart constraints	Controls input and output to the program. Uses various subroutines to calculate aerodynamic coefficients and centers of pressure for total missile and isolated components.
СМТРНІ	SEC.5.2.1	Calculates tail normal force coefficient in presence of a cylindrical body as a function of roll angle. (Angle of attack limited to 0 to 45 degrees).
CNTT	SEC.5.1.4	Calculates tail normal force coefficient of an isolated tail (angle of attack 0 to 180 degrees).
BRIT		Contains data required by several other Methodology subroutines. Data is taken from British Data Sheets. (Reference 3).
CNBOD	SEC.5.1.1	Calculates body alone normal force coefficient (angle of attack 0 to 180 degrees).
XCPBOD	SEC.5.1.2	Calculates body alone center of pressure measured in calibers from the nose. (Angle of attack 0 to 180 degrees).
IBTT	SEC.5.2.4	Calculates body normal carry over force coefficent.
XCPBTT	SEC.5.2.5	Calculates tail-to-body carry over normal force center of pressure.
XCPTBB	SEC.5.2.2	Calculates the tail chordwise center of pressure (upper and lower bound)/tail root chord, measured aft from root chord leading edge.

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
YCPTS	SEC.5.2.3	Calculates tail spanwise center of pressure for isolated tail.
XCPTT	SEC.5.1.5	Calculates chordwise center of pres- sure for isolated tail for roll angle = 0.
PHCC	and the same of the same of	Required by several other Methodology Subroutines.
AXIAL	SEC.5.1.3	Calculates the axial force coefficient for the missile body.
CSF	SEC.5.1.3	Calculates the skin friction coefficient for the missile body.
LOOKI		One-dimensional table look-up sub- routine.
LOOK2		Two-dimensional table look-up subroutine.
LOOK3		Three-dimensional table look-up subroutine.
INDEX		Required for subroutines LOOK1, LOOK2, and LOOK3.

A complete program listing follows.

## REFERENCES

- 1. Aiello, G.F., "Aerodynamic Methodology (Bodies With Arbitrary Roll Angles, Transonic and Supersonic)", Final report on USAMICOM Contract DAAH01-74-C-0621, OR 14,145, April 1976.
- Spring, D.J., Derrick, J.N., and Winn, G.C., "An Assessment of the Martin-Marietta High Angle of Attack Aerodynamic Methodology for Body-Tail Missiles", TR RD-76-33, US Army Missile Command, June 1976.
- 3. Royal Aeronautical Society, Data Sheets, Wings 5.01.03.03, 5.01.03. 04, 5.01.03.05, and 5.01.03.06.

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